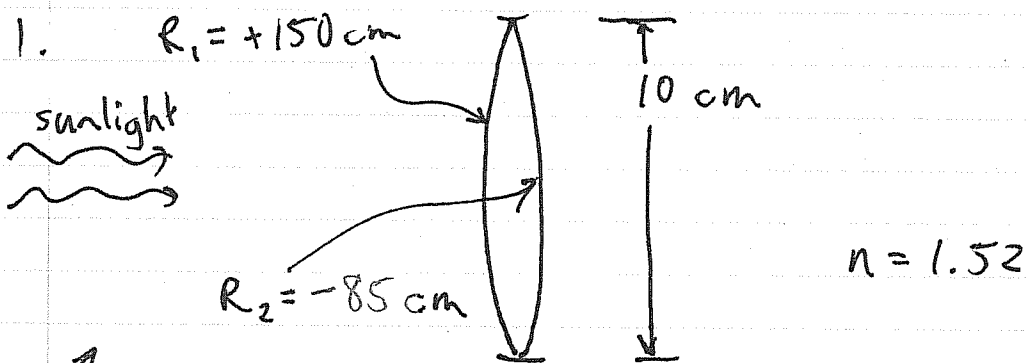


①

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Jason Harlow.

Using sign conventions
of Fig. 5.12 on pg. 156.

(a) Eq. 5.15: $\frac{1}{f} = (n-1) \left(\frac{1}{R_1} - \frac{1}{R_2} \right)$

$$f = \left[0.52 \left(\frac{1}{150} + \frac{1}{85} \right) \right]^{-1}$$

$$f = 104 \text{ cm}$$

(b) $s_o \gg (s_i, f) \Rightarrow s_i \approx f = 104 \text{ cm}$.

$$|M| = \frac{h_i}{h_o} = \frac{s_i}{s_o} \approx \frac{f}{s_o}$$

$$\Rightarrow h_i = \frac{h_o}{s_o} \cdot f = \frac{D_o}{1 \text{ A.U.}} \cdot f$$

$$h_i = \frac{1.4 \times 10^6 \text{ km}}{1.5 \times 10^8 \text{ km}} \cdot 104 \text{ cm} = 0.97 \text{ cm}$$

[Note: limit of

diffraction is $h_{\min} \approx \Delta\theta \cdot f = \left(\frac{1.22 \lambda}{D} \right) \cdot f$

$$h_{\min} \approx \frac{1.22 (550 \times 10^{-9} \text{ m})}{0.1 \text{ m}} \cdot 104 \text{ cm} = 7 \times 10^{-4} \text{ cm}$$

\rightarrow no problem]

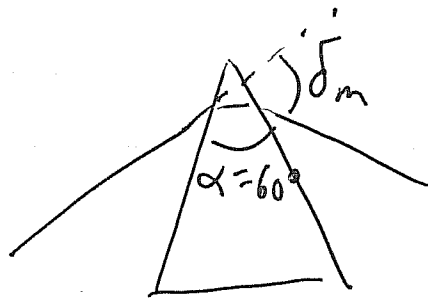
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2.



Eq. 5.54: $n = \frac{\sin[(\delta_m + \alpha)/2]}{\sin(\alpha/2)}$, solve for δ_m .

$$\sin\left[\frac{\delta_m + \alpha}{2}\right] = n \sin(\alpha/2)$$

$$\frac{\delta_m + \alpha}{2} = \sin^{-1}[n \sin(\alpha/2)]$$

$$\delta_m = 2 \sin^{-1}[n \sin(\alpha/2)] - \alpha$$

For $\alpha = 60^\circ$, $n_{\text{red}} = 1.525$

$$\delta_m = 2 \sin^{-1}[1.525 \sin 30^\circ] - 60^\circ$$

$$\delta_m = 39.37018^\circ$$

For $\alpha = 60^\circ$, $n_{\text{blue}} = 1.535$

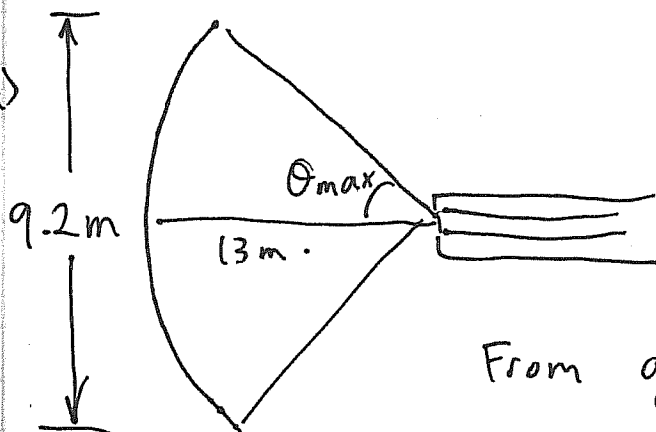
$$\delta_m = 40.25984^\circ$$

Difference: $\Delta\delta_m = 0.89^\circ$

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3.
(a)



$$f = \frac{R}{2} = 13 \text{ m}$$

core: $n_f = 1.620$
cladding $n_c = ?$

From geometry

$$\tan \theta_{max} = \frac{(9.2/2)}{13}$$

$$\theta_{max} = 19.49^\circ$$

From Eq. 5.64 $\therefore NA = (n_f^2 - n_c^2)^{1/2}$

and $NA = n_0 \sin \theta_{max}$, $n_0 = 1$ in air.

$$\Rightarrow \sqrt{n_f^2 - n_c^2} = \sin \theta_{max}$$

$$n_f^2 - n_c^2 = \sin^2 \theta_{max}$$

$$n_c = \sqrt{n_f^2 - \sin^2 \theta_{max}}$$

$$= \sqrt{1.620^2 - (\sin 19.49^\circ)^2}$$

$$\boxed{n_c = 1.585} \leftarrow \text{maximum cladding index.}$$

(b)

Eq. 5.65 :

$$\frac{P_o}{P_i} = 10^{-\alpha L/10}$$

$$\alpha = 0.85 \text{ dB/km}$$

$$L = 50 \text{ m} \left(\frac{1 \text{ km}}{1000 \text{ m}} \right) = 0.05 \text{ km.}$$

$$\frac{P_o}{P_i} = 0.9903$$

$$\boxed{99.03\%}$$

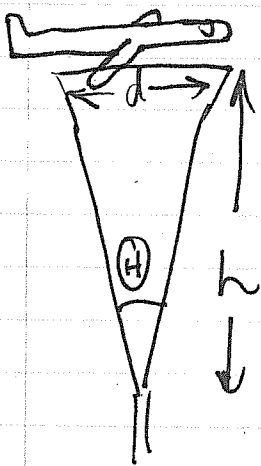
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4. (a) From the equation above Eq. 13.19, the full angular width of a beam is



$$\theta = \frac{2.44 \lambda}{D} \quad *$$

$$\theta \approx \frac{d}{h} \Rightarrow d = \theta \cdot h$$

$$d = \frac{2.44 \lambda}{D} \cdot h$$

$$d = \frac{2.44 (532 \times 10^{-9} \text{ m})}{4 \times 10^{-3} \text{ m}} \cdot 500$$

$$d = 0.16 \text{ m} = \boxed{16 \text{ cm diameter}}$$

$$(b) \quad I = \frac{P}{A} = \frac{P}{\pi r^2} = \frac{P}{\pi (D/2)^2}$$

$$= \frac{0.7 \times 10^{-3} \text{ W}}{\pi (0.16/2)^2} = \boxed{0.034 \frac{\text{W}}{\text{m}^2}}$$

* If you use $\theta = 0.637 \frac{\lambda}{D}$ from pg. 595

this is $\theta = 1.27 \frac{\lambda}{D}$ \Rightarrow (a) 8.4 cm diameter
 (b) 0.13 W/m²
 Eq. 13.19.