

TRACKING DETECTORS

OBJECTIVE: OBSERVE TRAJECTORY OF CHARGED PARTICLE WITH AS LITTLE INTERFERENCE AS POSSIBLE.

→ USE A "THIN" DETECTOR

SCINTILLATORS ($\sigma \sim \text{cm}$)

GAS BASED DETECTORS ($\sigma \lesssim \text{mm}$)

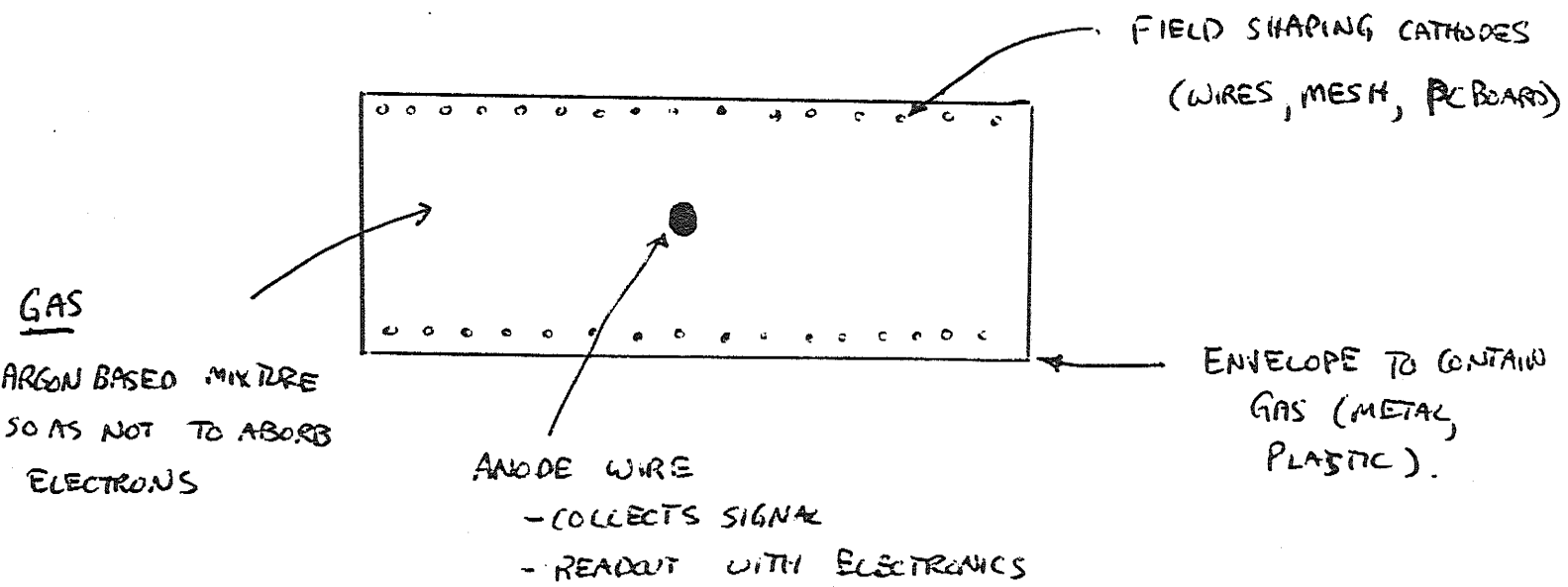
SILICON DETECTORS ($\sigma \approx 10 \mu\text{m}$)

START WITH GAS BASED DETECTORS:

- MULTI-WIRE PROPORTIONAL CHAMBER
- DRIFT CHAMBER
- TIME PROJECTION CHAMBER.

OFTEN USE COMBINATIONS OF CHAMBERS TO MEASURE DIFFERENT PROPERTIES OF A PARTICLE.

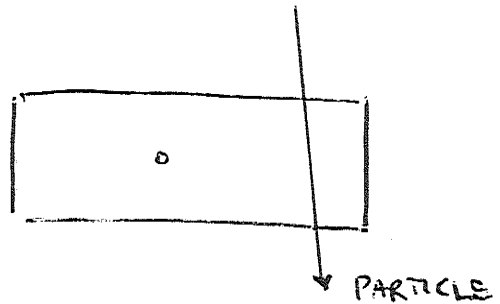
SCHEMATIC OF A WIRE CHAMBER



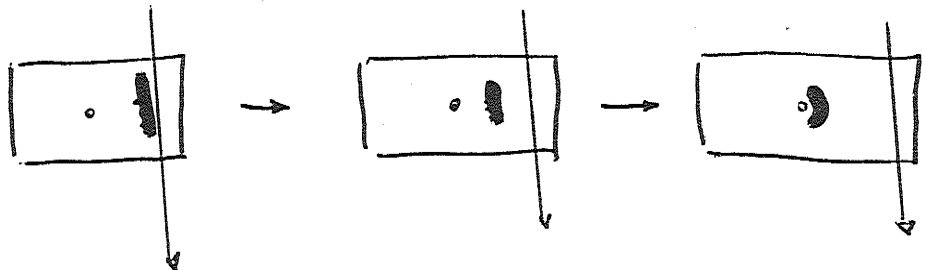
THREE ESSENTIAL STAGES

① IONISATION

ELECTRONS FROM GAS ARE
DISTURBED BY PASSAGE OF
CHARGED PARTICLE ($dE/dx!$)



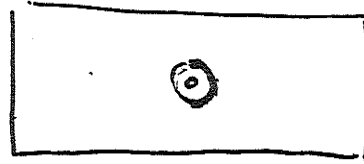
② DRIFT



IONISED ELECTRONS FORCED BY THE DRIFT FIELD TO MIGRATE TOWARDS
THE ANODE WIRE. A "DIRECTED" RANDOM WALK.

③

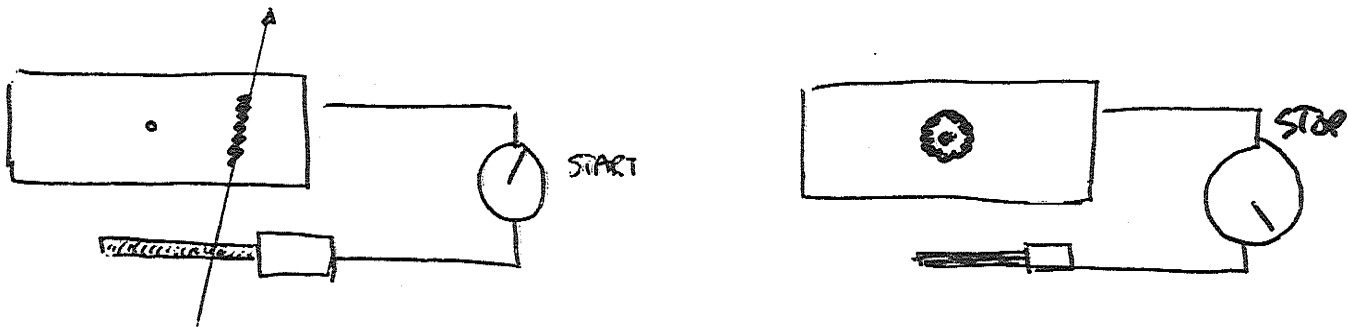
AMPLIFICATION



IN THE HIGH FIELD REGION NEAR THE ANODE WIRE THE IONISATION ELECTRONS GAIN ENOUGH ENERGY BETWEEN COLLISIONS TO THEMSELVES IONIZE.

THIS RESULTS IN AN AVALANCHE WITH GAINS UP TO 10^7 POSSIBLE.

DRIFT AND DIFFUSION OF ELECTRONS



DRIFT CHAMBER WORKS BY MEASURING THE TIME IT TAKES FOR ELECTRONS TO ARRIVE AT THE ANODE.

AS ELECTRONS DRIFT DIFFUSION CAUSES ORIGINALLY WELL DEFINED CLOUD TO SPREAD OUT \Rightarrow ARRIVES AT ANODE "FAINTER" \Rightarrow LESS WELL DEFINED INTERPRETATION OF ORIGINAL POSITION

LIMIT ON RESOLUTION OF DETECTOR.

③

IONISATION TURNS 1 NEUTRAL ATOM

↳ 1 ELECTRON (small mass & size)
1 POSITIVE ION (LARGE & HEAVY)

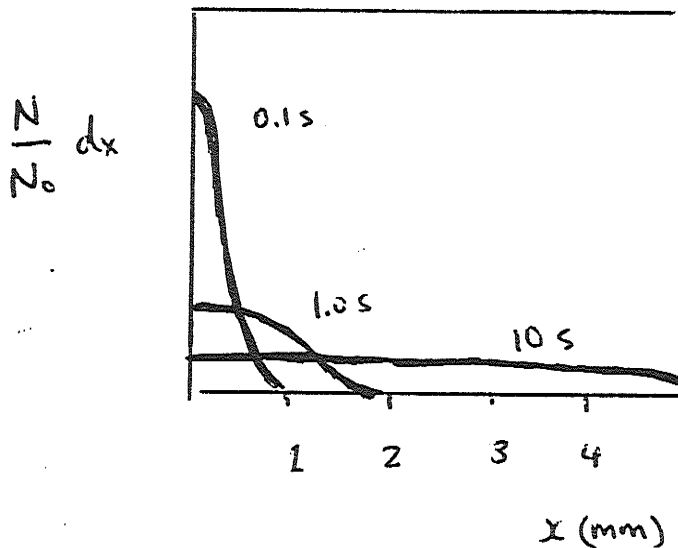
UNDER THE INFLUENCE OF DRIFT FIELD THEY MOVE AWAY FROM THEIR BIRTH PLACE. THIS IS A RANDOM WALK (MULTIPLE COLLISIONS) OR DIFFUSION

IN ABSENCE OF EXTERNAL FIELD THEY FOLLOW A TIME DEPENDENT GAUSSIAN SPATIAL DISTRIBUTION

$$\frac{dN}{N} = \frac{1}{\sqrt{4\pi Dt}} e^{-x^2/4Dt} dx$$

$$\sigma^2 = 2Dt$$

D = Diffusion coefficient
t = time



DIST'N OF IONS IN AIR

$$R.M.S. = \sqrt{2} \sqrt{Dt} \quad \text{IN ANY DIREC}$$

CHARACTERISTICS OF DIFFUSION

- MEAN FREE PATH BETWEEN COLLISIONS

IONS $\approx 10^{-5}$ cm

ELECTRONS $\approx 10^{-6}$ cm

- AVERAGE VELOCITY BETWEEN COLLISIONS:

$5 \times 10^4 - 2 \times 10^5$ cm/s (IONS)

10^7 cm/s (ELECTRONS)

IN PRESENCE OF AN ELECTRIC FIELD:



$\frac{dx_1}{dt}$ = THERMAL VELOCITY

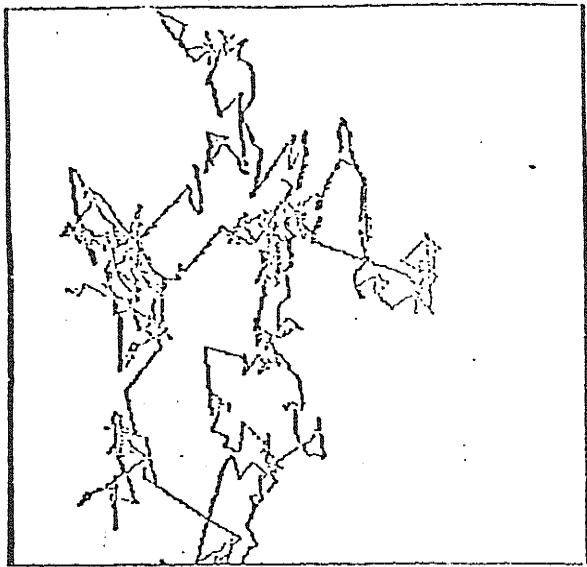
$w \equiv \frac{dx_2}{dt}$ = DRIFT VELOCITY

IONS DRIFT VELOCITY DEPENDS ON $\frac{|\vec{E}|}{P}$ TO VERY HIGH $|\vec{E}|$

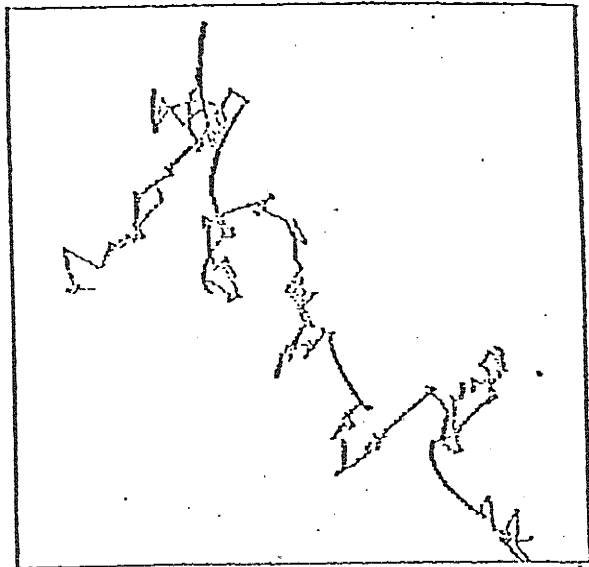
$$w = \frac{\mu |\vec{E}|}{P}$$

μ = MOBILITY SPECIFIC TO ION SPECIES AND SURROUNDING GAS

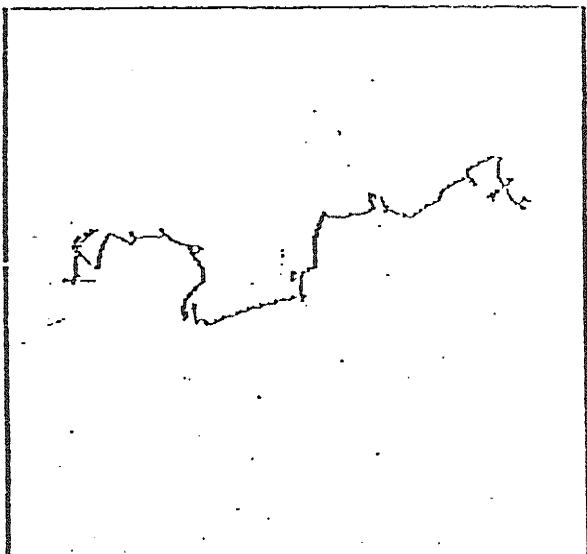
P = PRESSURE OF SURROUNDING GAS.



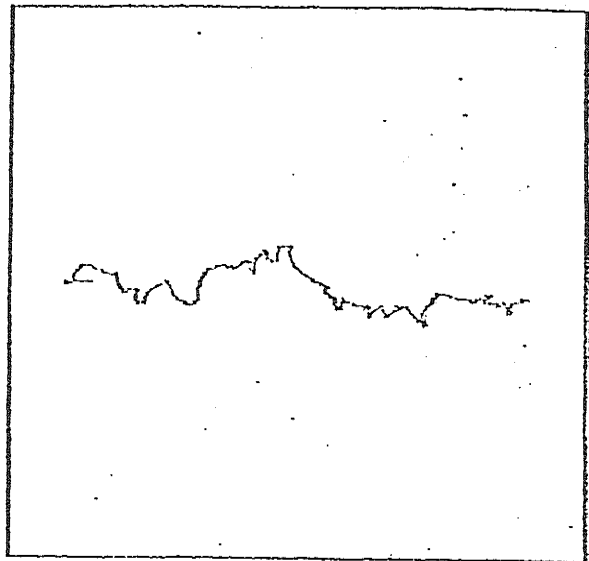
E/P=10



E/P=100



E/P=500



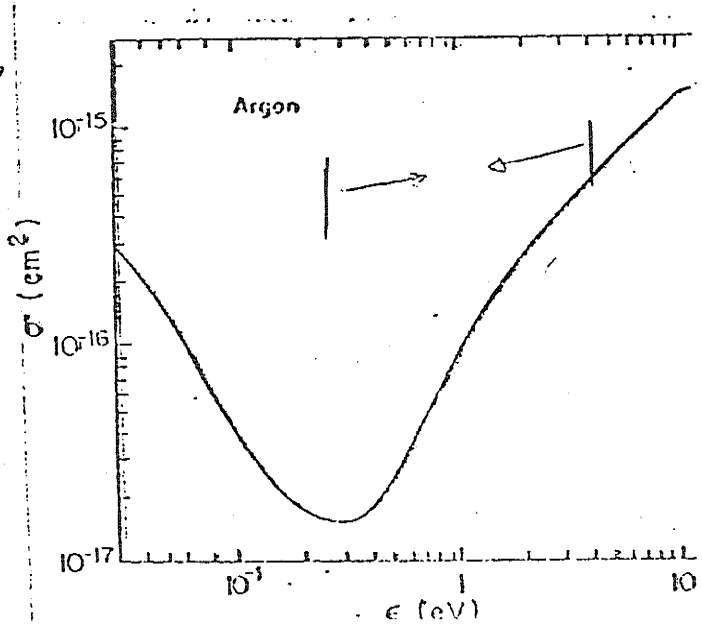
FIELD DIRECTION →

E/P=1500

ELECTRONS

MOBILITY IS NOT CONSTANT

MEAN FREE PATH DEPENDS ON ELECTRON INTERACTION CROSS-SECTION WHICH IN TURN DEPENDS ON ATOMIC LEVELS ETC.

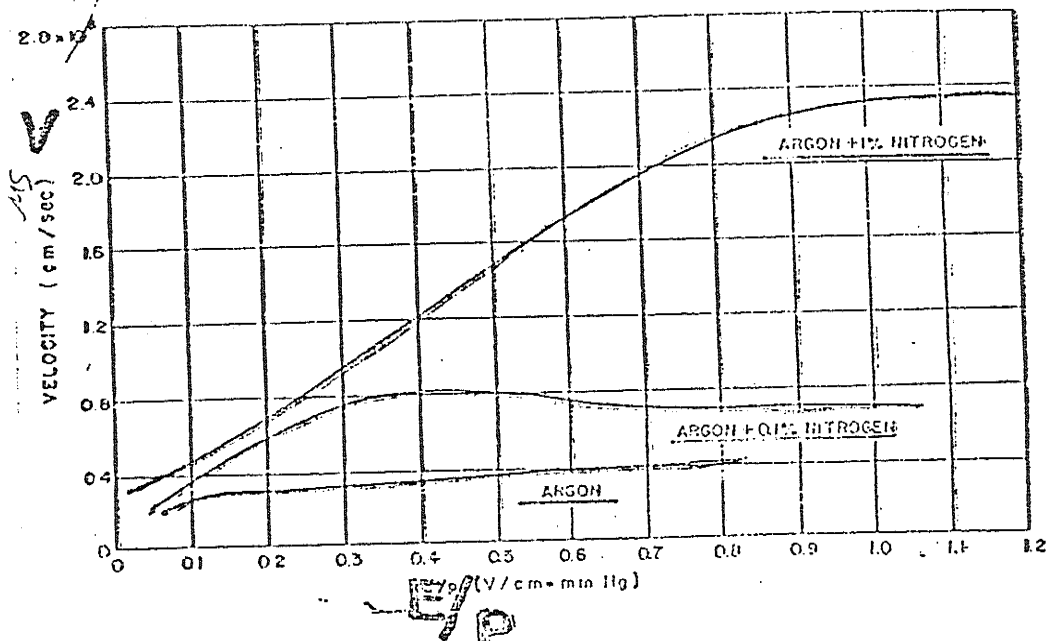


RAMSAUER CROSS-SECTION FOR ELECTRONS IN ARGON

LOW $\sigma \Rightarrow$ LONG MEAN FREE PATH

\Rightarrow EXTRA DIFFUSION

THESE CROSS-SECTIONS ARE GAS DEPENDENT



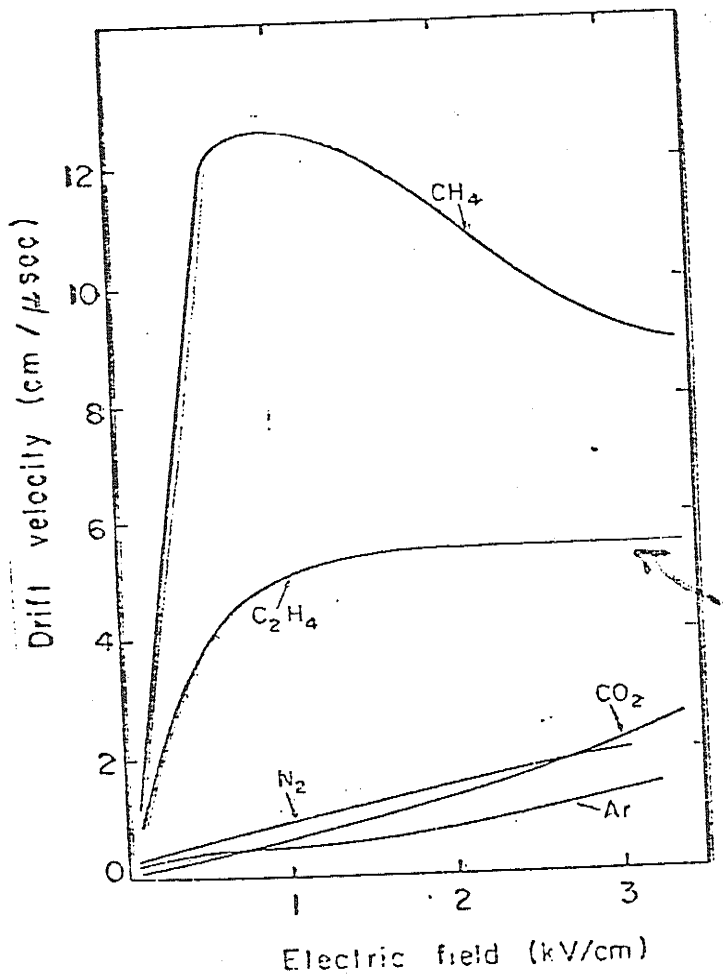
SMALL ADDITIONS \Rightarrow BIG EFFECTS

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SATURATED DRIFT VELOCITIES

As $|E|$ INCREASES SO DOES ELECTRON ENERGY

THIS CAN INCREASE INTERACTION CROSS-SECTION REDUCING THE MEAN FREE PATH AND HENCE DRIFT VELOCITY



THIS CAN LEAD TO A SATURATION OF DRIFT VELOCITY

IDEAL FOR DRIFT CHAMBERS WHERE YOU WANT A PRECISE d vs t RELATIONSHIP TO DETERMINE DRIFT DISTANCE

DIFFUSION LIMIT TO SPATIAL ACCURACY

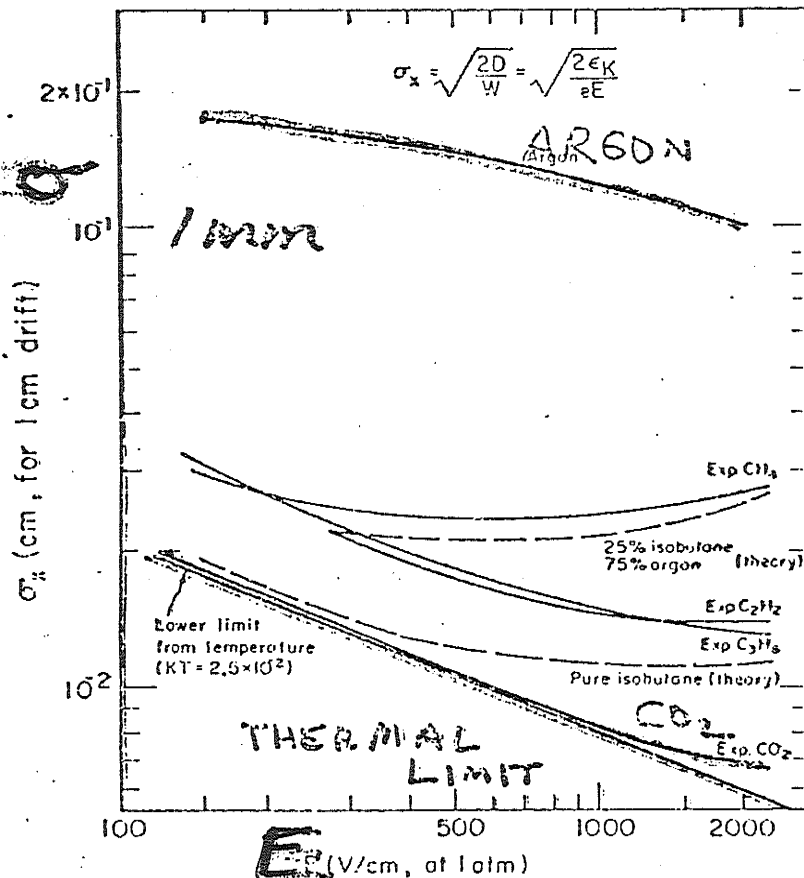
RECALL $\sigma^2 = 2Dt$

DEFINE $\sigma(1\text{cm}) = \sqrt{\frac{2D}{W}}$

$\therefore t = \frac{1\text{cm}}{W}$

NB $\sigma(x) = \sigma(1\text{cm}) \sqrt{x}$

$\sigma(1\text{cm})$ IS ^{ANOTHER} A FIGURE OF MERIT FOR ACCURACY IN A DRIFT CHAMBER



NOTE THAT $\sigma(1\text{cm})$ DEPS SLIGHTLY FOR INCREASING $|E|$

HIGHEST ACCURACY FOR "COOL GASES" LIKE CO₂ WHERE DIFFUSION SMALL

PRICE TO PAY IS DRIFT VELOCITY NOT SATURATED.

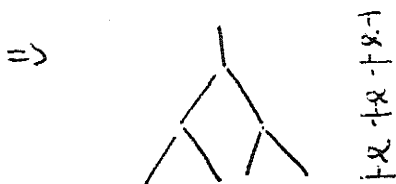
AMPLIFICATION (AVALANCHE THEORY)

AS $|\vec{E}|$ INCREASES ELECTRONS GAIN ENOUGH ENERGY TO THEMSELVES, IONISE.

SIMPLE CASCADE MODEL

→ ASSUME UNIFORM $|\vec{E}|$

→ CONSTANT MEAN FREE PATH \propto



IF ELECTRONS IONISE IN $s \propto$ THEN WE GET AN EXPONENTIAL CASCADE

$$dn = n \alpha dx$$

α = DOUBLING LENGTH OF CASCADE

$$\Rightarrow n = n_0 e^{\alpha x}$$

NUMBER OF ELECTRON IN CASCADE

$$M = \frac{n}{n_0} = e^{\alpha x}$$

MULTIPLICATION FACTOR OR GAIN

FOR NON-UNIFORM FIELDS (IE. AROUND A WIRE $|\vec{E}| \propto \frac{1}{r}$)

$$\alpha = \alpha(E) = \alpha(x)$$

$$M = \exp \int_{x_1}^{x_2} \alpha(x) dx$$

↳ TOWNSEND COEFFICIENT.

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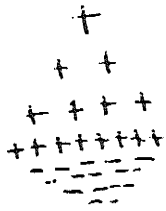
AVALANCHE SHAPE

POSITIVE IONS MOVE SLOWLY

HALF WERE CREATED IN LAST MEAN FREE PATH

⇒ TEAR DROP SHAPE

IONS

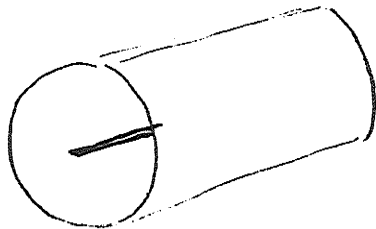


ELECTRONS

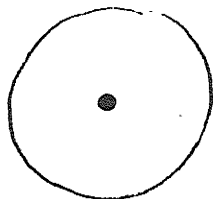
PROPORTIONAL CHAMBERS

- FOR "CORRECT" HV THE SIZE (INTEGRATED CHARGE) OF THE DETECTED PULSE IS PROPORTIONAL TO THE ENERGY DEPOSITED IN THE COUNTER

SIMPLEST EXAMPLE



TIN WIRE (ANODE) INSIDE A GROUNDED METAL CYLINDER (CATHODE).



→ a
← b ←

FOR $a < r < b$

$$E = \frac{CV_0}{2\pi\epsilon_0} \frac{1}{r}$$

$$V = \frac{CV_0}{2\pi\epsilon_0} \ln\left(\frac{r}{a}\right)$$

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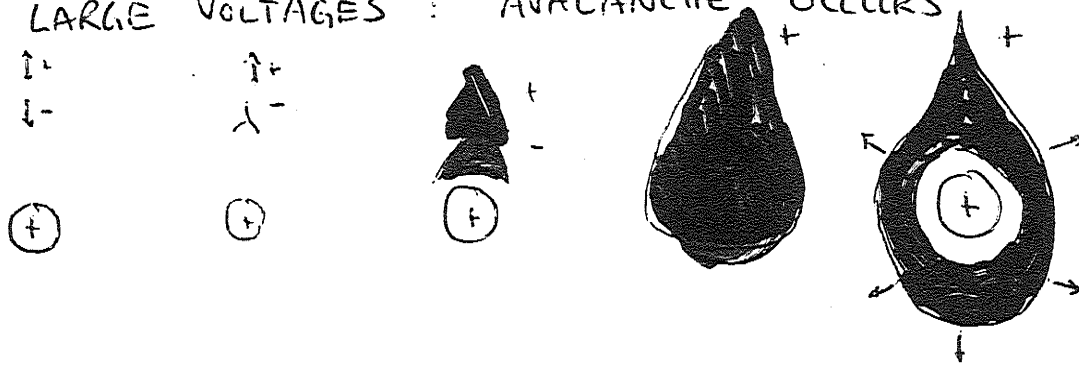
TYPICALLY $a \approx 10 - 50 \mu\text{m}$

FOR LOW VOLTAGES : ENOUGH TO ATTRACT IONISED
ELECTRONS TO WIRE BUT NOT ENOUGH FOR
AMPLIFICATION

$$\text{SIGNAL} = V = \frac{q}{C} = \frac{n e}{C}$$

$n = \#$ of
primary
electrons

FOR LARGE VOLTAGES : AVALANCHE OCCURS



DIFFUSION CAUSES AVALANCHE TO SURROUND WIRE

ELECTRONS ARE COLLECTED WITHIN ~ 1 ns

POSITIVE IONS MIGRATE SLOWLY TOWARDS CATHODE

$$W = \frac{\mu E}{P}$$

\Rightarrow ION VELOCITY FALLS AWAY
FROM WIRE

SIMPLE ELECTROSTATICS

MOVING A CHARGE Q A DISTANCE dr IN A SYSTEM
OF CAPACITANCE Cl ($C = \text{CAPACITANCE / UNIT LENGTH}$)

$$\Rightarrow \text{INDUCED SIGNAL} \quad dv = \frac{Q}{ClV_0} \frac{dV}{dr} dr.$$

$V_0 = \text{TOTAL VOLTAGE BETWEEN ANODE \& CATHODE}$

$\frac{dV}{dr} = \text{VOLTAGE GRADIENT (LOCALLY)}$ aka. **ELECTRIC FIELD.**

CONSIDER SIGNAL FROM CHARGES PRODUCED WITHIN A
DISTANCE λ OF THE WIRE. (ie $r = \lambda + a$)

ELECTRON CONTRIBUTION:

$$V^- = \frac{-Q}{lCV_0} \int_a^{a+\lambda} \frac{dV}{dr} dr = -\frac{Q}{2\pi\epsilon_0 l} \ln\left(\frac{a+\lambda}{a}\right)$$

POSITIVE ION CONTRIBUTION:

$$V^+ = \frac{Q}{lCV_0} \int_{a+\lambda}^b \frac{dV}{dr} dr = -\frac{Q}{2\pi\epsilon_0 l} \ln\left(\frac{b}{a+\lambda}\right)$$

TOTAL SIGNAL:

$$V = V^+ + V^- = -\frac{Q}{2\pi\epsilon_0 l} \left[\ln\left(\frac{a+\lambda}{a}\right) + \ln\left(\frac{b}{a+\lambda}\right) \right]$$

$$V^+ + V^- = \frac{-Q}{2\pi\epsilon_0 l} \ln\left(\frac{b}{a}\right) = \frac{Q}{2\pi\epsilon_0 l} \quad \text{OK}$$

RATIO: $\frac{V^-}{V^+} = \frac{\ln(a+\lambda) - \ln(a)}{\ln(b) - \ln(a+\lambda)} \approx 1\%$

$a = 10 \mu\text{m}$
 $\lambda = 1 \mu\text{m}$
 $b = 10 \text{mm}$
(TYPICAL VALUES)

\Rightarrow ELECTRON CONTRIBUTION TO SIGNAL ≈ 0 .

TIME DEVELOPMENT OF SIGNAL

CONSIDER ONLY POSITIVE IONS.

$$V(t) = - \int_0^t v(t') dt' = \frac{-Q}{2\pi\epsilon_0 l} \ln\left(\frac{r(t)}{a}\right)$$

\uparrow
 $t=0$ when ions at
 $r=a$.

$$\frac{dr}{dt} = w = \frac{\mu E}{P} = \frac{\mu}{P} \frac{CV_0}{2\pi\epsilon_0} \frac{1}{r}$$

$$\int_a^r r' dr' = \frac{\mu}{P} \frac{CV_0}{2\pi\epsilon_0} \int_0^t dt$$

$$\frac{r^2}{2} - \frac{a^2}{2} = \frac{\mu}{P} \frac{CV_0}{2\pi\epsilon_0} t$$

$$\Rightarrow r(t) = \left(a^2 + \frac{\mu}{P} \frac{C V_0 t}{\pi \epsilon_0} \right)^{1/2}$$

$$\Rightarrow V(t) = \frac{-Q}{4\pi \epsilon_0 l} \ln \left(1 + \frac{\mu \epsilon V_0 t}{\pi \epsilon_0 P a^2} \right)$$

$$= \frac{-Q}{4\pi \epsilon_0 l} \ln \left(1 + \frac{t}{t_0} \right) \quad \textcircled{\text{I}}$$

LET T BE THE TOTAL DRIFT TIME OF POSITIVE IONS (ie time to get from $r=a \rightarrow r=b$)

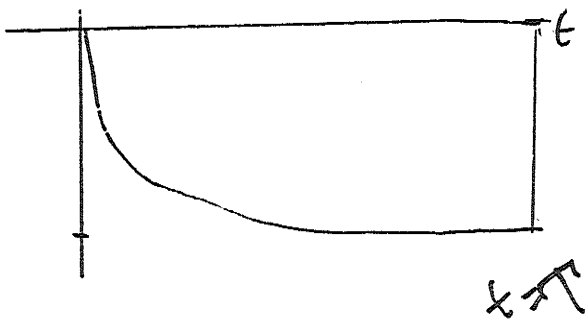
$$r(T) = b = \left(a^2 + \frac{\mu}{P} \frac{C V_0 T}{\pi \epsilon_0} \right)^{1/2}$$

II

$$T = \frac{\pi \epsilon_0 P}{\mu C V_0} (b^2 - a^2)$$

$$= 550 \mu\text{s.}$$

$$\begin{aligned} a &= 10 \mu\text{m} \\ b &= 8 \text{mm} \\ C &= 8 \text{pF/m} \\ \mu &= 1.7 \frac{\text{cm}^2}{\text{S} \cdot \text{V} \cdot \text{AT}} \\ &\quad \text{(ARGON)} \\ V_0 &= 3 \text{kV} \end{aligned}$$



THIS IS A VERY LONG TIME (EVEN IN SLOW EXPERIMENTS LIKE LEP)

CROSS-CHECK:

$$\begin{aligned}V_{\max} &= \sqrt{T} \\&= \frac{-Q}{4\pi\epsilon_0 l} \ln\left(1 + \frac{b^2 - a^2}{a^2}\right) \\&= \frac{-Q}{2\pi\epsilon_0 l} \ln\left(\frac{b}{a}\right) \quad \checkmark\end{aligned}$$

WHAT ABOUT TIME TO GET

$$V = V_{\max} / 2$$

$$V\left(\frac{t}{2}\right) = \frac{V_{\max}}{2} = \frac{-Q}{4\pi\epsilon_0 l} \ln\left(\frac{b}{a}\right) = \frac{-Q}{4\pi\epsilon_0 l} \ln\left(1 + \frac{t}{t_0}\right)$$

$$\begin{aligned}\Rightarrow \ln\left(1 + \frac{t_{1/2}}{t_0}\right) &= \ln\left(\frac{b}{a}\right) & t_{1/2} &= t_0 \left(\frac{b}{a} - 1\right) \\& & &= \pi \frac{a^2}{(b^2 - a^2)} \left(\frac{b - a}{a}\right)\end{aligned}$$

From (I) and (II)

$$t_0 = \pi \frac{a^2}{(b^2 - a^2)}$$

$$\Rightarrow t_{1/2} = \pi \frac{a}{(a + b)}$$

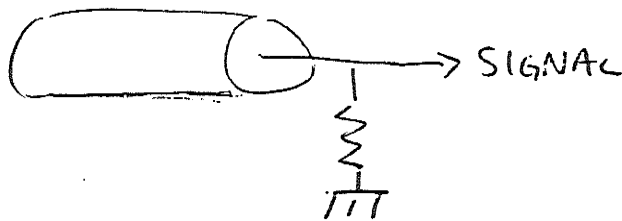
$$a = 10 \mu\text{m} \quad b = 10 \text{ mm}$$

$$\Rightarrow t = \pi / 1000$$

THUS GET $\frac{1}{2}$ THE SIGNAL IN $\frac{1}{1000^{\text{th}}}$ OF THE TIME
THIS IS MUCH MORE PRACTICAL.

LEADS TO A WHOLE ART OF POST-CHAMBER
PULSE SHAPING,

SIMPLEST REALISATION: RC - CIRCUIT



$C =$ INTRINSIC COUPLING
CAPACITANCE

$$8 \text{ pF/m} \sim 1 \text{ m} \text{ br} \\ \Rightarrow 8 \text{ pF}$$

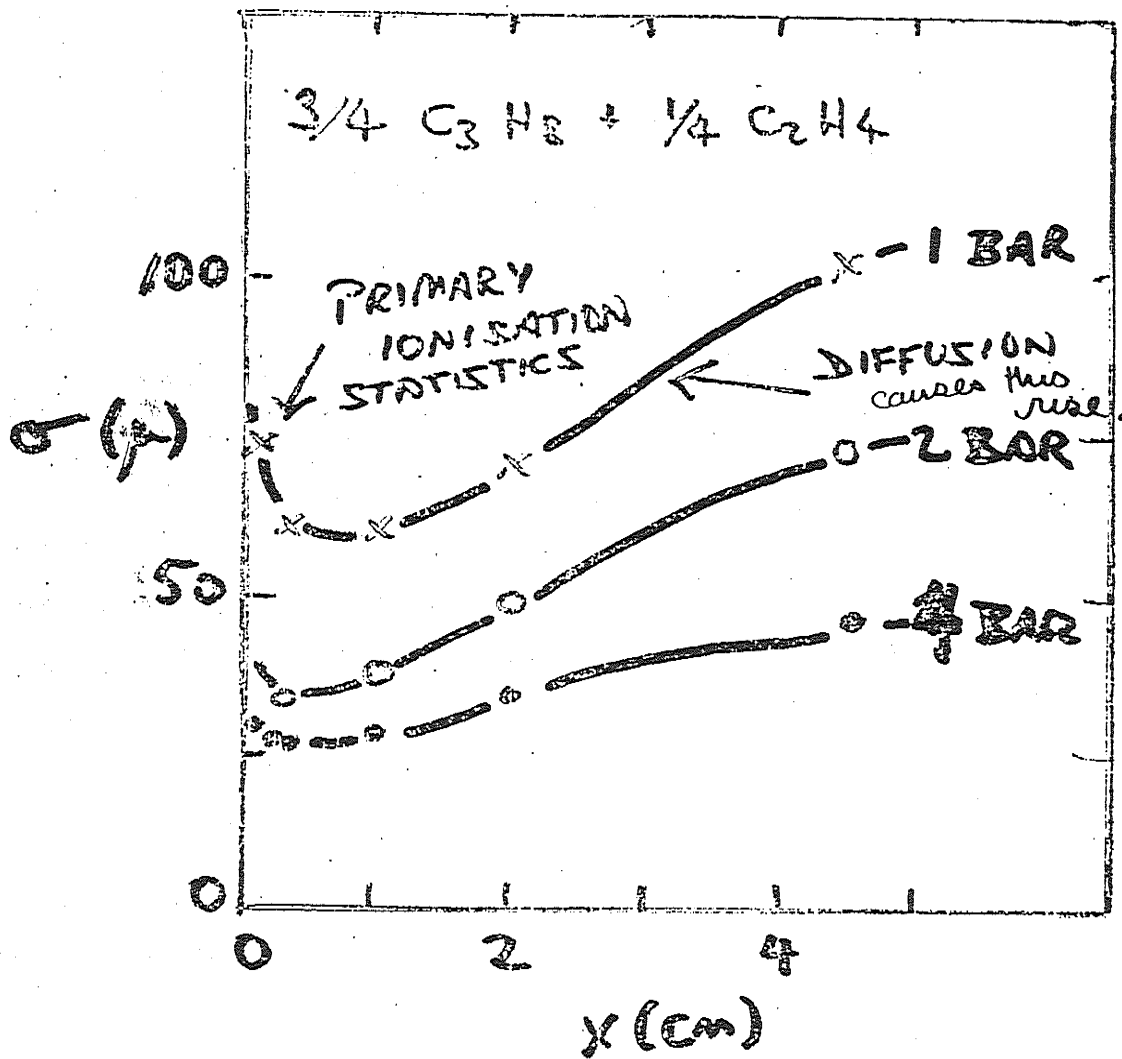
$R =$ TERMINATOR
 $\approx 1 \text{ M}\Omega$

$$\Rightarrow RC = 8 \mu\text{s}.$$

DRIFT CHAMBER RESOLUTION

vs.

GAS PRESSURE



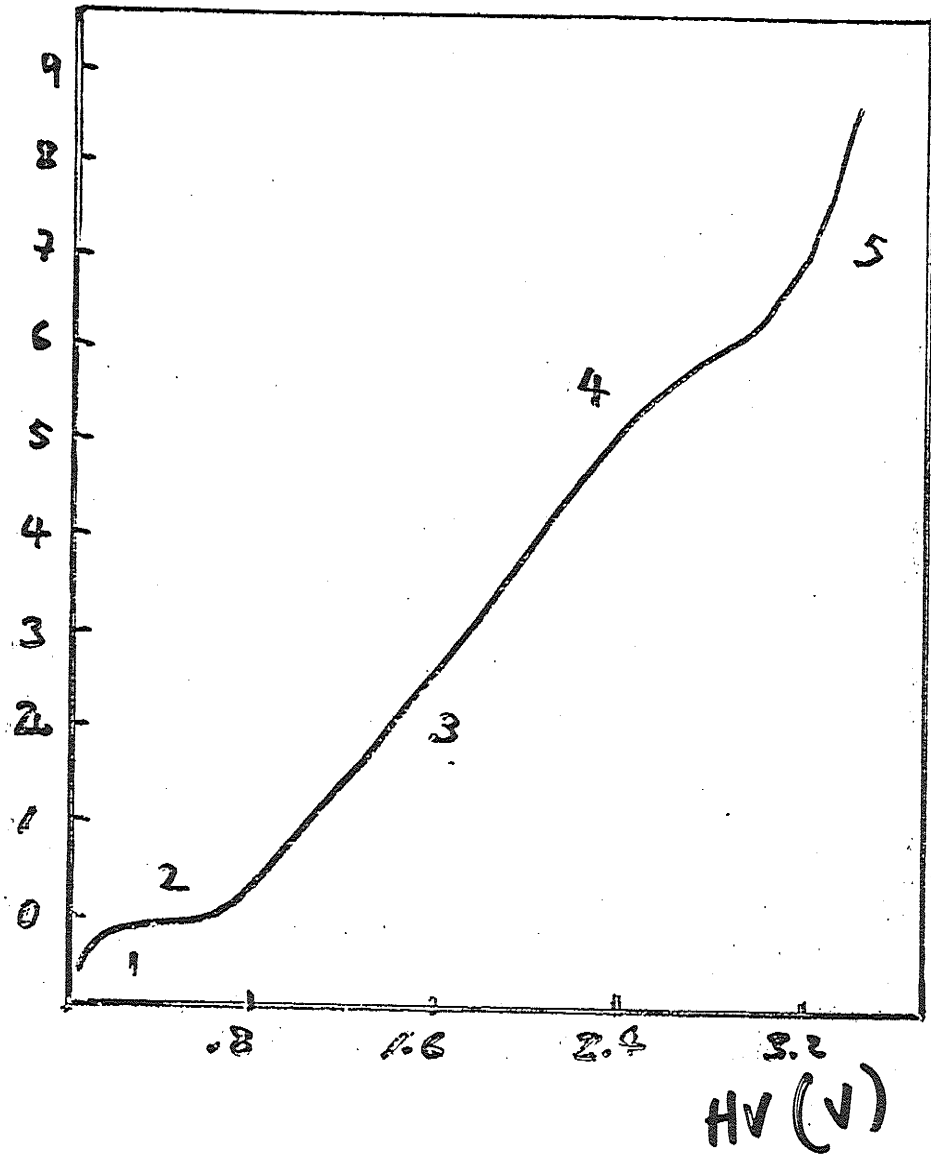
AT LOW PATH LENGTHS ACTUAL IONISATION
"CLUMPS" (POISSON STATISTICS) WHICH
CAN CAUSE RESOLUTION FLUCTUATIONS

Skip in 2024

TRACKING CHAMBERS (Continued)

CHAMBER GAIN OPERATING REGIONS

log(M)



REGION 1

NO AMPLIFICATION - SOME SIGNAL LOST DURING DRIFT!

REGION 2

ION CHAMBER MODE - NO AMPLIFICATION, BUT ALL PRIMARY IONISATION COLLECTED.

2

REGION 3 - PROPORTIONAL MODE PULSE SIZE CORRELATED TO DEPOSITED CHARGE GAINS UP TO 10^4 .

REGION 4 - LIMITED STREAMER MODE

GAIN TOO HIGH TO PRESERVE PROPORTIONALITY. POSITIVE ION CLOUD FROM CHARGES ARRIVING EARLY SCREEN THE ANODE, REDUCE \Rightarrow REDUCE GAIN FOR SUBSEQUENT ARRIVALS

\rightarrow ADVANTAGE FASTER OPERATION WHERE SIGNAL PULSE HEIGHT NOT IMPORTANT. (OR SMALL GAP OPERATION)

REGION 5 - GEIGER - MÜLLER MODE

\rightarrow AVALANCHE GENERATES PHOTONS
 \hookrightarrow LONG MEAN FREE PATH.

\rightarrow AVALANCHE SPREADS ALL ALONG ANODE
 \Rightarrow ENORMOUS PULSE

- CHAMBER IS DEAD FOR A LONG TIME.

- ADVANTAGE IS NO SOPHISTICATED READOUT ELECTRONICS IS NEEDED.

CHOICE OF GAS

- START WITH A NOBLE GAS
 - NOT ELECTRONEGATIVE (GOOD FOR DRIFTING)
 - LARGE TOWNSEND COEFFICIENT
- PICK ONE WITH HIGH SPECIFIC IONISATION
⇒ LOTS OF IONS / CM OF PARTICLE TRACK
- ARGON CHEAPER THAN XENON OR KRYPTON.

GAIN LIMIT

$10^3 - 10^4$ FOR ARGON

DURING AVALANCHE MANY EXCITED IONS (CREATED ONLY 11 eV ABOVE SIMPLE IONISATION)

⇒ 11 eV PHOTON WILL BE EMITTED.

PHOTON TYPICALLY HAS MEAN FREE PATH > SIZE OF CELL ⇒ CAN TRAVEL TO CATHODE AND EJECT ELECTRON (WORK FUNCTION OF COPPER ~ 8 eV).

THIS ELECTRON WILL RETURN TO ANODE

⇒ RUNAWAY DISCHARGE.

NEED QUENCHERS

QUENCHERS

POLYATOMIC MOLECULES HAVE ROTATIONAL AND VIBRATIONAL MODES - THESE CAN ABSORB PHOTONS

METHANE (CH_4) ABSORBS IN 8-14 eV RANGE

TYPICALLY ARGON - CH_4 IN 80-20 MIX IS SUITABLE.

POLYMERISATION

- IN THE PROCESS OF ABSORBING PHOTONS POLYATOMIC QUENCHERS CAN DISSOCIATE

→ POLYMERS

- POLYMERS ARE ATTRACTED TO ANODE OR CATHODE WHERE THEY CAN BUILD UP OVER TIME

- RESULTS IN AGEING → BUILD UP OF INSULATORS ON ANODE OR CATHODE
⇒ NON-UNIFORM ELECTRIC FIELDS.

CAN USE NON-POLYMERISING ADDITIVES LIKE METHYLAL (Ar-Isobutane (C_4H_{10})) BUBBLED THROUGH METHYLAL WAS A STANDARD CHOICE)

NOW USE ARGON-ETHANE (MUCH LESS POLYMERISING)

EXAMPLES OF POLYMER BUILDUP

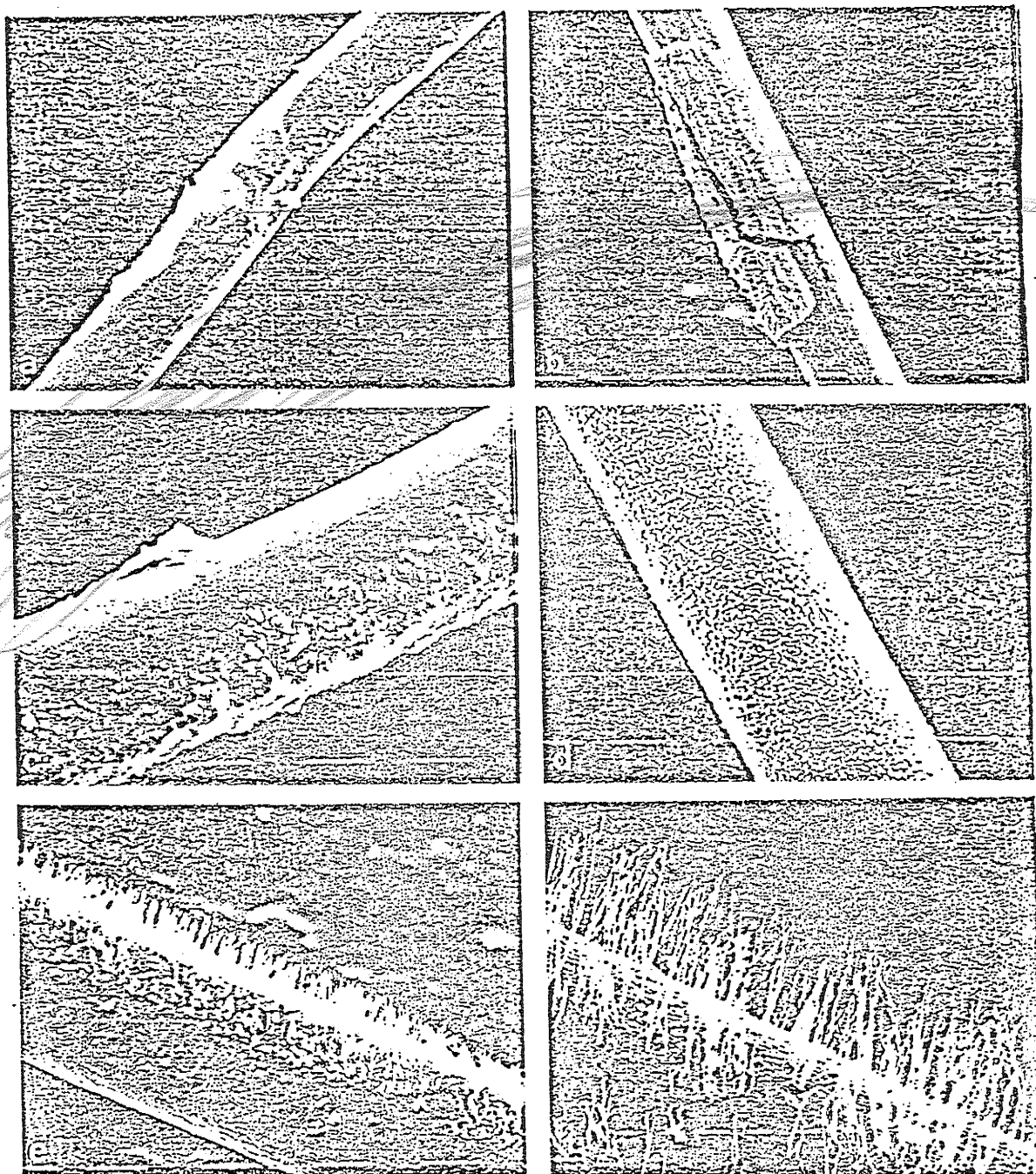
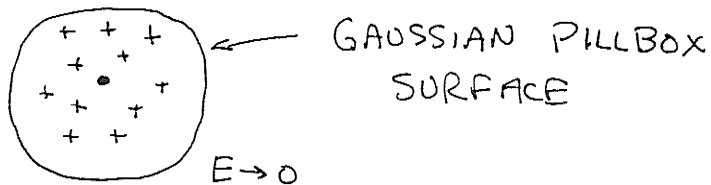


Fig. 6. Deposits on anode wires. (a-c) from the G10 chambers: (a) Ar/C₂F₆; (b) +methylal; (c) Ar/CO₂; (d) from the perspex chamber; (e,f) from the G10 chamber and cold trap.

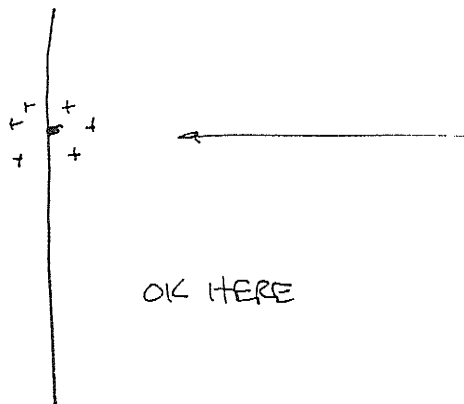
DEATH IF TOTAL SIGNAL (INCLUDING
GAIN) > 1 C/cm

SPACE CHARGE GAIN LIMITATION

POSITIVE IONS SHIELD ELECTRIC FIELD OF WIRE



NOMINAL FIELD ONLY RESTORED AFTER IONS → CATHODE (100's μ s).



PROPORTIONAL MODE
⇒ LOCAL DEAD REGIONS

GEIGER MODE
⇒ WHOLE TUBE DEAD

HIGH RATE ENVIRONMENTS (eg. CDF run 2, ATLAS)

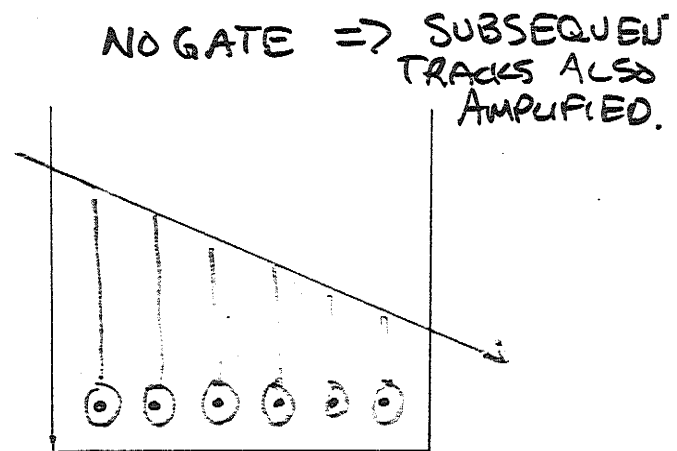
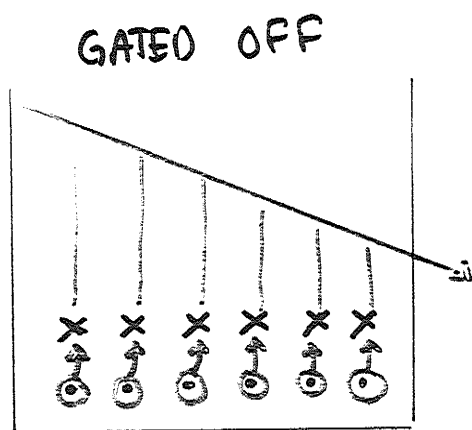
- EVEN PROPORTIONAL MODE MAY NOT BE GOOD ENOUGH
- MANY SMALL DEAD REGIONS CAN STILL GIVE FINITE INEFFICIENCIES.
- EVEN MORE SERIOUS FOR A DRIFT CHAMBER
 - DRIFT FIELD BECOMES UNPREDICTABLY DISTORTED.

SOLUTIONS TO SPACE CHARGED PROBLEMS

- RUN AT VERY LOW PROPORTIONAL GAIN
=> FEWER POSITIVE IONS

BUT SMALLER SIGNALS

- WORK WITH SMALLER ANODE/CATHODE GAPS
=> FASTER ION MIGRATION
- GATE OFF THE AMPLIFICATION REGION.



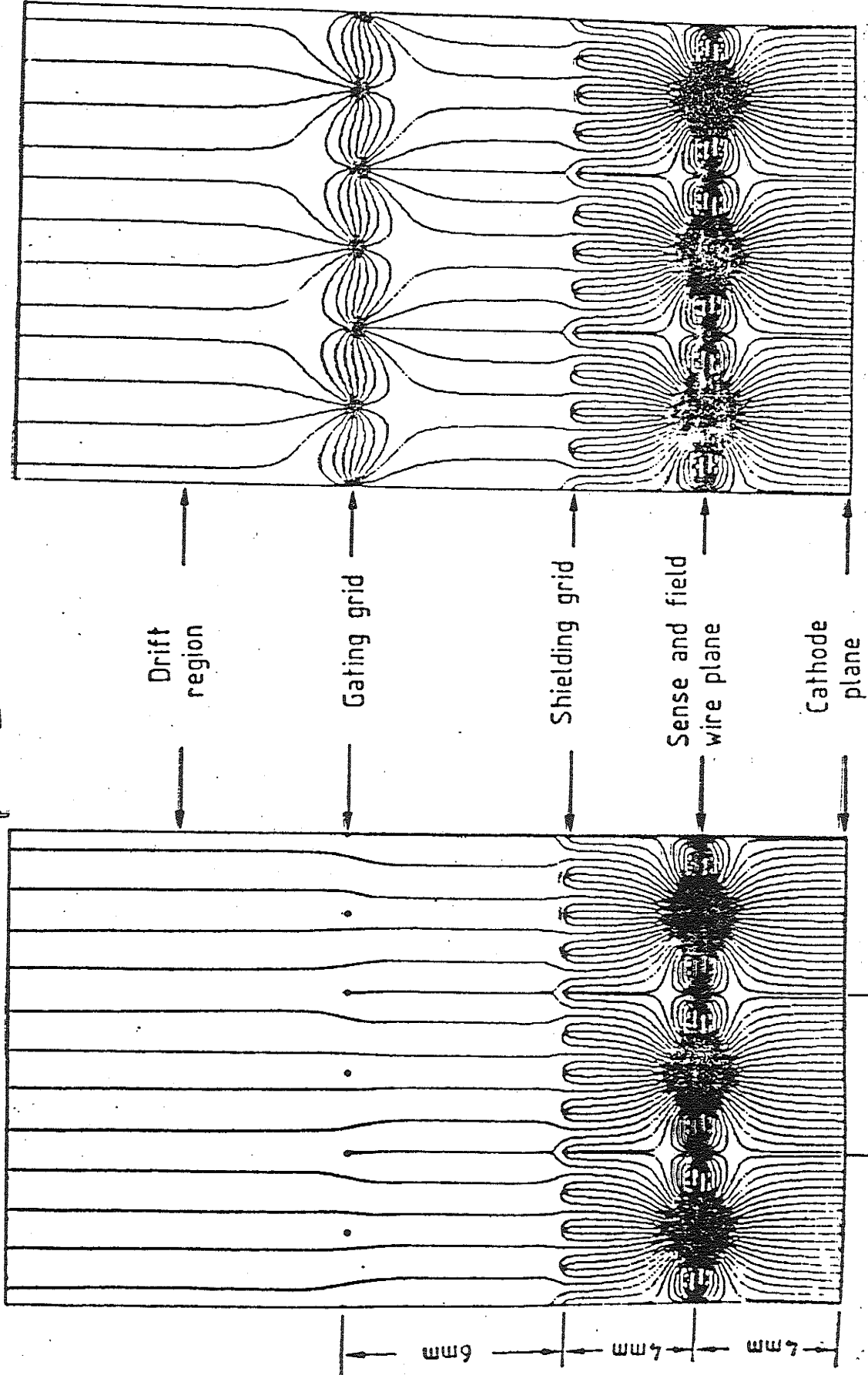
- ANODE WIRES
- × GATING WIRES

CHANGING VOLTAGES ON GRID BY $\pm 50V$ BLOCKS OFF AMPLIFICATION REGION => IONS ONLY HAVE TO "RETURN" TO GATING GRID.

APPLYING ΔV WHEN "INTERESTING TRACKS" ARE PRESENT => ONLY "USEFUL SIGNALS" AMPLIFIED.

ALEPH TPC GATES

GATE IS OPENED AND CLOSED BY A SQUARE WAVE TRAIN. IONS ARE FORCED ONTO NEGATIVE WIRE.



CLOSED GATE

Fig 2(a)-2(b)

OPEN GATE

Include in 2024

SOME SPECIFIC EXAMPLES

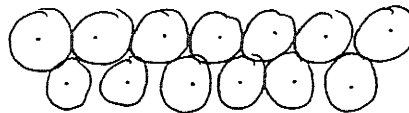
MULTI-WIRE PROPORTIONAL CHAMBERS (MWPC's)

- MOST-OFTEN USED IN FIXED TARGET GEOMETRIES
BUT STILL USED IN:

- BEAM CHAMBERS
- MUON DETECTORS
- SOME FINE GRANULARITY CALORIMETER

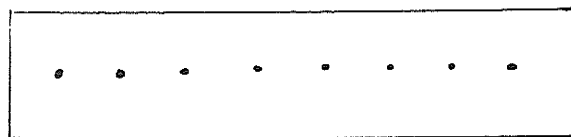


INTER-TUBE
INEFFICIENCIES



BETTER, BUT
BULKY.

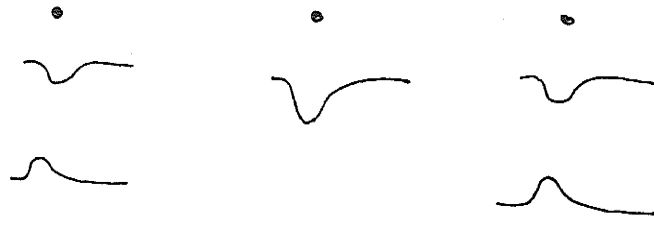
1967 CHARPAK



PUT MANY WIRES
IN SINGLE GAS
VOLUME.

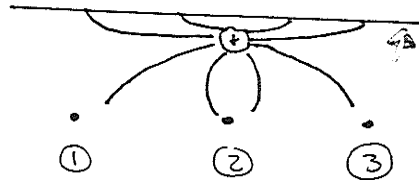
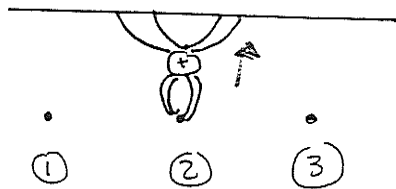
STUMBLING BLOCK WAS BELIEF THAT SIGNAL ON
ONE WIRE WOULD INDUCE SIGNALS ON ALL
NEIGHBORING WIRES (CAPACITIVE CROSS-TALK).

IN FACT NEGATIVE "CROSS-TALK" SIGNALS ARE
CANCELLED BY MOVEMENT OF POSITIVE IONS
INDUCING POSITIVE SIGNALS ON NEIGHBORING
WIRES.



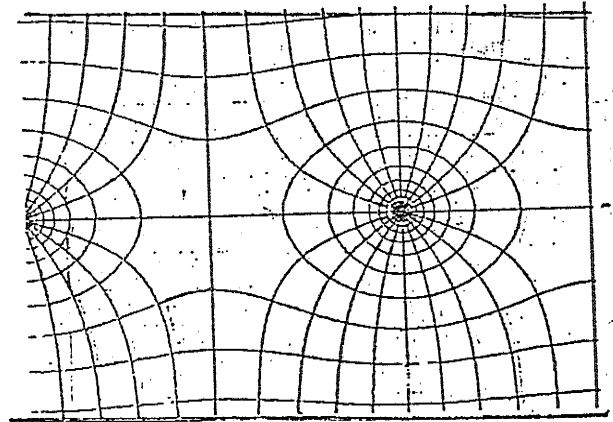
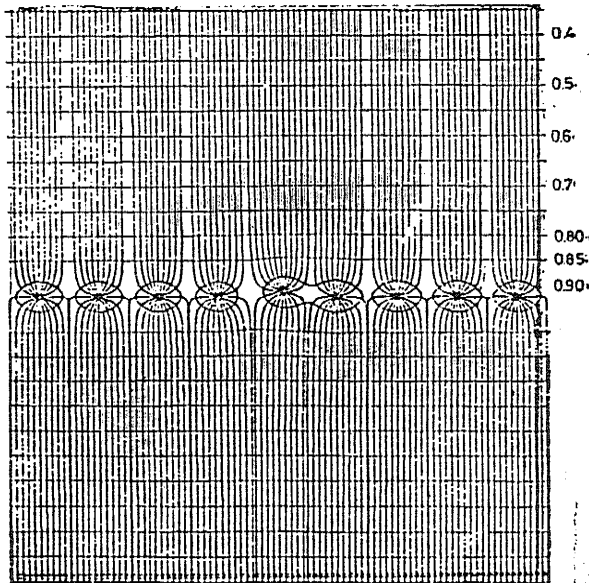
ION INDUCED SIGNAL

CROSS-TALK



THE BOTTOM LINE IS THAT THE ACTUALLY WORK.

TYPICAL FIELD CONFIGURATION

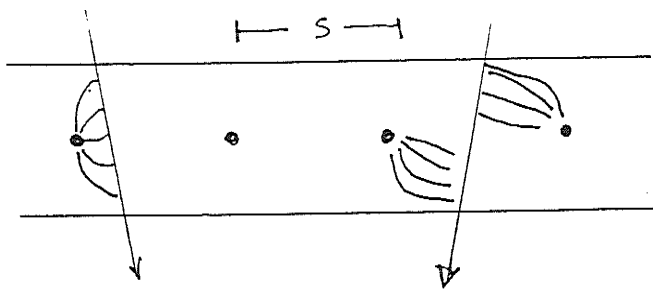


WIRE SPACING 2 mm
WIRE DIAMETER 20 μ m



MWPCs (CONTINUED)

- NO TIMING INFORMATION RECORDED
- POSITION IS TAKEN AS THAT OF STRUCK WIRE (SOMETIMES TWO WIRES SHARE SIGNAL \Rightarrow TAKE MIDPOINT BETWEEN THE TWO STRUCK WIRES).



THUS:

RESOLUTION $\sim s$

$$\sigma = \text{RMS} = \sqrt{\frac{\int_{-s/2}^{s/2} (x - \bar{x})^2 dx}{\int_{-s/2}^{s/2} dx}}$$

e.g. $\bar{x} = 0$

$$= \sqrt{\frac{\left. \frac{x^3}{3} \right|_{-s/2}^{s/2}}{\left. x \right|_{-s/2}^{s/2}}}$$

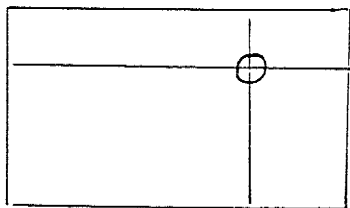
$$= \frac{s}{\sqrt{12}}$$

PITCH $\sqrt{12}$ IS THE STANDARD AGAINST WHICH

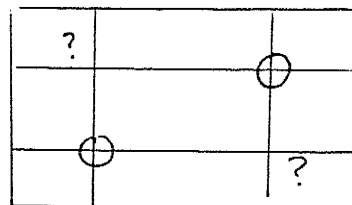
ALL WIRE CHAMBER PERFORMANCES ARE
JUDGED.

CHAMBER SYSTEMS

- Two consecutive planes can be used to define a point

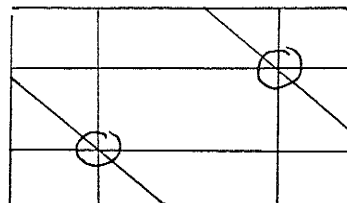


FOR MULTIPLE TRACKS



x, y

NEED TO ADD A THIRD NON-PARALLEL PLANE



x, y
z
U or V.

ANOTHER WAY TO GAIN ADDITIONAL INFORMATION IS TO SEGMENT AND READOUT THE CATHODE

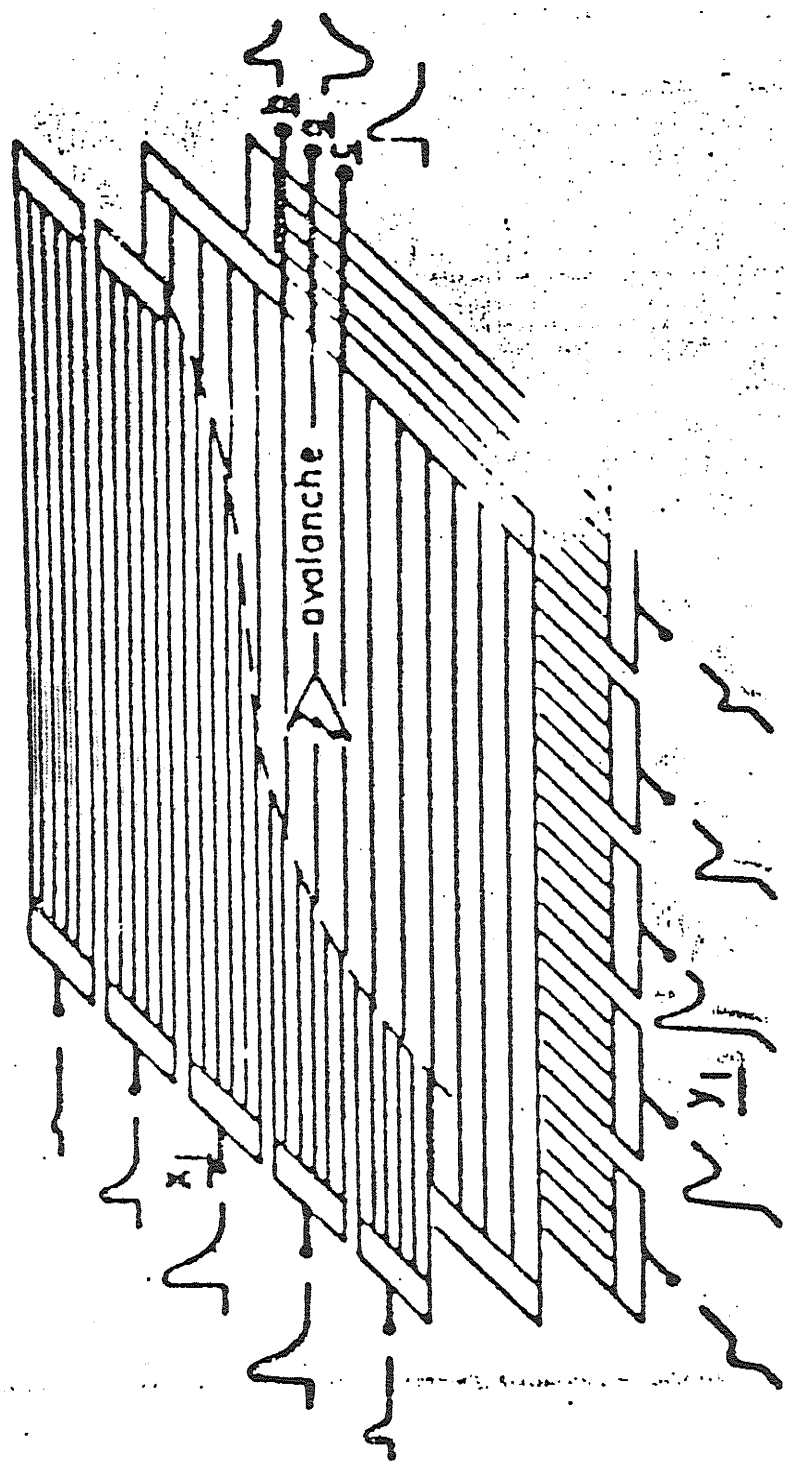
ANALANCHE ON WIRE CAUSES POSITIVE PULSES ON NEIGHBORING CATHODE ELECTRODES.

NOTE: TYPICALLY CELL THICKNESS $\sim 4 \times$ PITCH (CAPACITANCE $\frac{1}{2}$ PRIMARY IONISATION)

\Rightarrow SIGNAL SPREADS OVER $\approx 4 \times$ LARGER AREA.

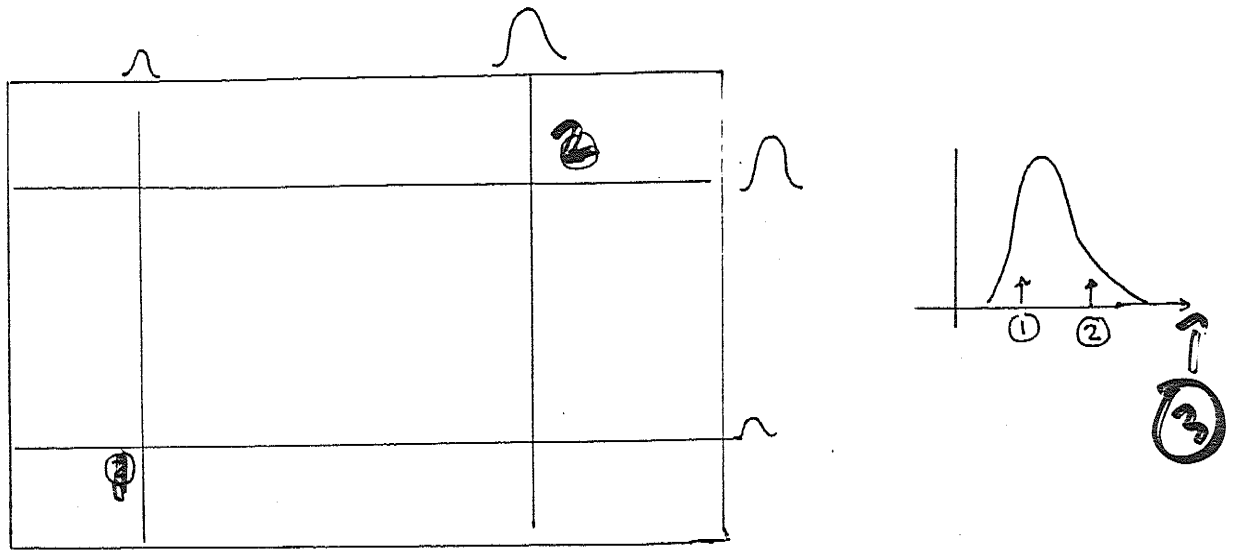
SEGMENTED CATHODES

CATHODE TYPICALLY 3-4 x FURTHER AWAY FROM WIRE THAN WIRE SPACING (s) => SIGNALS MORE SPREAD OUT. USE CENTRE OF GRAVITY MEASUREMENT.



MULTIPLE TRACKS WITH CATHODE READOUT

Not
ATLAS-SCT



CORRELATE LANDAU FLUCTUATIONS

ONLY POSSIBLE WHEN SIGNALS RESULT FROM
THE SAME AVALANCHE. IE CATHODE AND
ANODE OF SAME CHAMBER.

IN PRACTICE THIS PROCEDURE IS LIMITED BY
THE S/N OF THE READOUT. IF THE

NOISE IN THE READOUT SYSTEM IS COMPARABLE
TO THE PROBABLE LANDAU FLUCTUATIONS THEN
VERY FEW AMBIGUITIES CAN BE RESOLVED
THIS WAY.

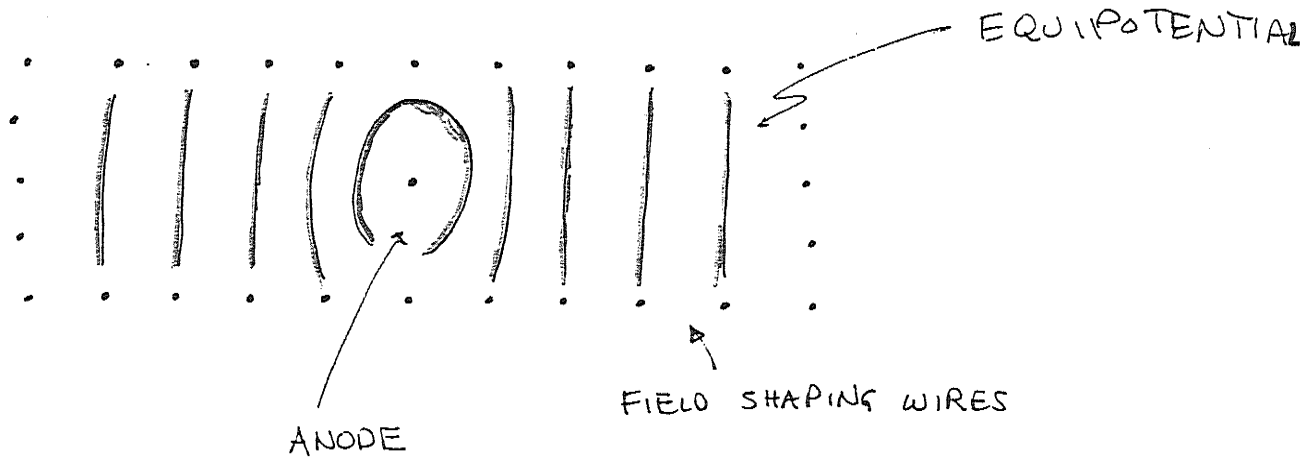
DRIFT CHAMBERS

BASIC IDEA : MEASURE ARRIVAL TIME OF CHARGE AT ANODE (W.R.T. EXTERNAL TRIGGER) TO

1) IMPROVE POSITION RESOLUTION

OR

2) EXTEND SENSITIVE AREA OF A SINGLE WIRE / REDUCE READOUT CHANNELS.



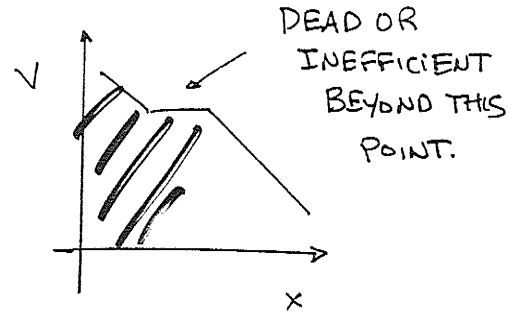
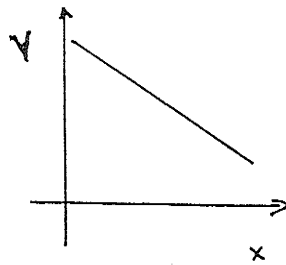
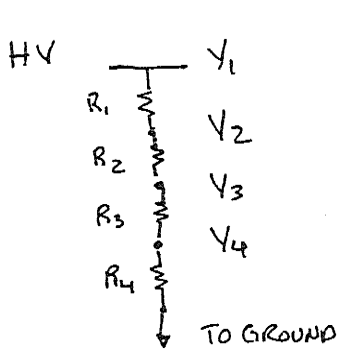
NEED UNIFORM DRIFT FIELD TO HAVE A RELIABLE d vs. t RELATIONSHIP.

ALWAYS LIMITED BY CHANGING FIELD IN AMPLIFICATION REGION.

- TO A LESSER EXTENT VERY LONG DRIFTS (FROM EDGE OF CELL) ALSO PROBLEMATIC.

Skip in 2024

POSSIBLE PROBLEMS WITH FIELD SHAPING



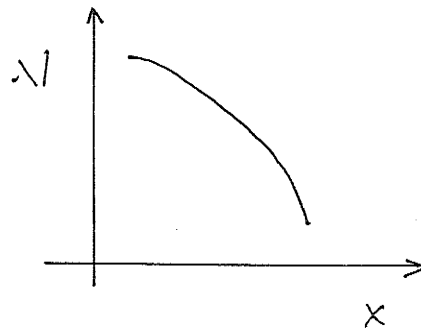
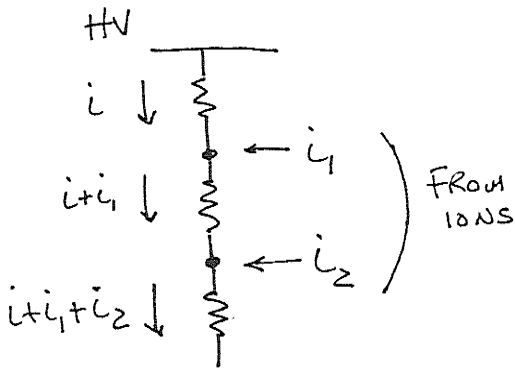
IF R_N SHORTS

$$V_N = V_{N+1}$$

IF R_N OPEN

WHOLE CELL DEAD

IN HIGH RATE OPERATION IONS BEGIN TO NEUTRALISE ON DIVIDER CHAIN



NEED HIGH CURRENT CHAIN:

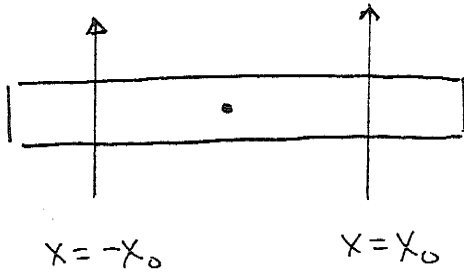
$$i \gg i_1, i_2.$$

ALSO CAN HAVE PROBLEMS IF FIELD SHAPING WIRES NEAR INSULATING MATERIAL (CHAMBER WALLS) POSITIVE IONS CAN CHARGE UP NEAR FIELD WIRES \Rightarrow UGLY DRIFT FIELD.

②

Include in 2024

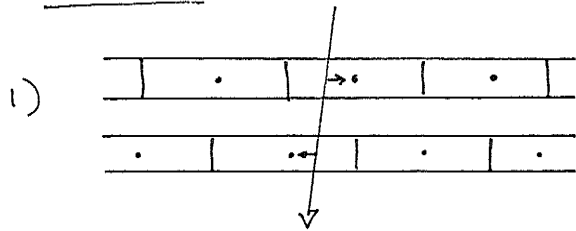
LEFT - RIGHT AMBIGUITY



$$t = |x|/w = x_0/w$$

WHICH SIDE?

SOLUTIONS



t_1

t_2

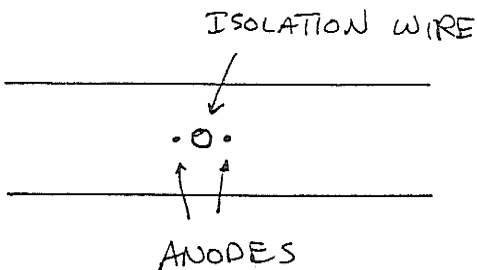
CLOSER THE BETTER
ESPECIALLY FOR ANGLED
TRACKS

FOR NORMAL (\perp) TRACKS

$$t_1 + t_2 = \text{CONSTANT} = \frac{\text{CELL SIZE}}{w}$$

\Rightarrow CALIBRATION.

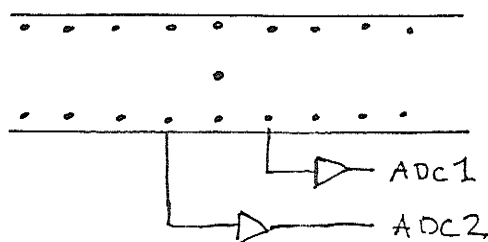
2)



2 ANODE WIRES

2x READOUT ELECTRONICS.

3)

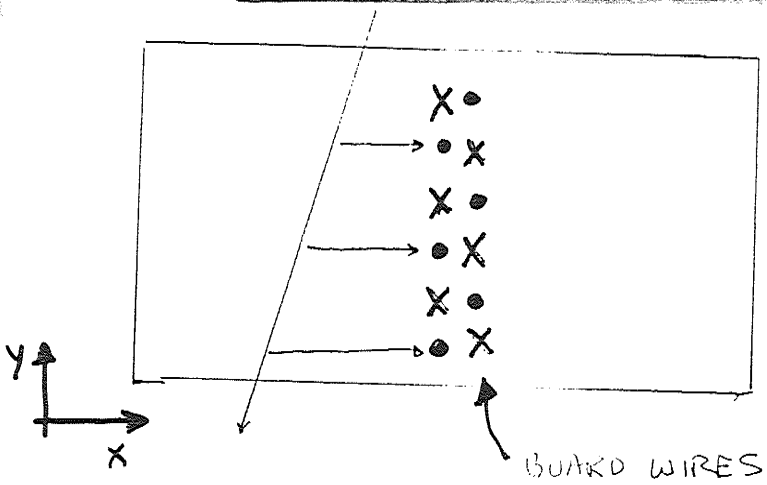


READOUT LAST
FIELD SHAPING WIRES

3x ELECTRONICS

③

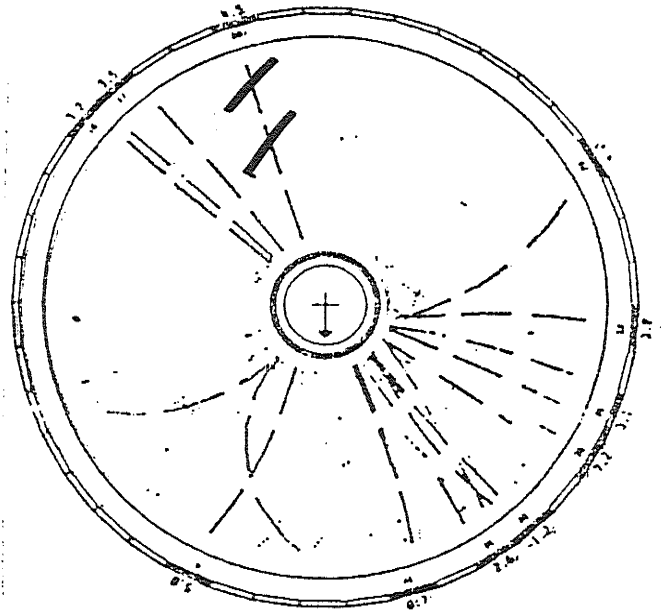
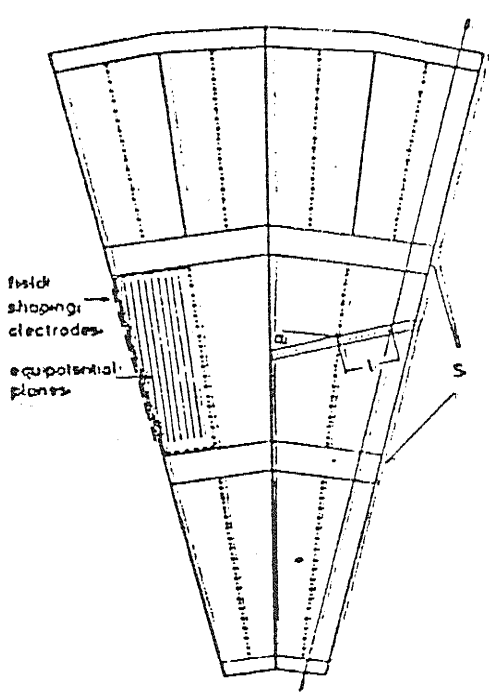
MULTIPLE ANODE DRIFT CELLS



3 ANODES FOR LEFT

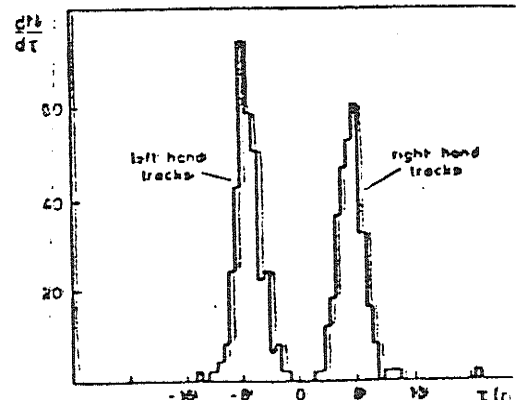
3 ANODES FOR RIGHT

SLOPE $\frac{1}{3}$ POSITION FROM
A SINGLE CELL



JET CHAMBER

(JADE, OPAL, ...)



④

left/right separation > position resolution

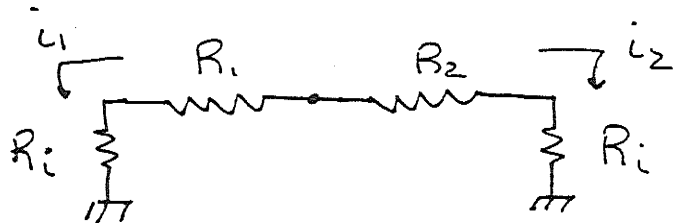
Skip in 2024

DETERMINING THE THIRD COORDINATE

x GIVEN BY DRIFT TIMING
 y GIVEN BY WIRE POSITION
 z ?

CHARGE DIVISION

INTEGRATE i_1, i_2
 $\rightarrow Q_1, Q_2$



$$i_1(R_i + R_1) = i_2(R_i + R_2)$$

$$L$$

$$z$$

$$\frac{Q_1}{Q_2} = \frac{R_i + R_2}{R_i + R_1} = \frac{R_i + \rho z}{R_i + \rho(L-z)}$$

TAKE $z_i = R_i / \rho$

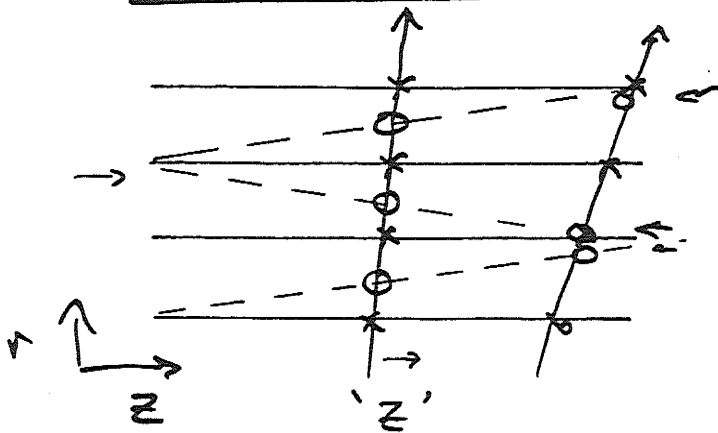
EQUIVALENT LENGTH OF WIRE
 IN AMPLIFIER INPUT

$$\Rightarrow z = z_i \frac{(Q_1 - Q_2)}{(Q_1 + Q_2)} + L \frac{Q_1}{(Q_1 + Q_2)}$$

↑
 MAKE SMALL WITH HIGH
 ρ WIRE OR LOW R_i
 AMPLIFIER

TYPICALLY δQ_i GOOD ENOUGH TO MAKE $\sigma_z \lesssim 10\% L$
 0.5% in OPAL ≈ 1 cm in 2.0m WIRES.

STEREO WIRES (CDF, ZEUS, OPAL VTX)



ALTERNATING LAYERS

- 0
- +θ
- 0
- θ
- 0
- etc.

TYPICALLY ANGLES OF A FEW DEGREES
 ($6^\circ \approx 100 \text{ mrad} \Rightarrow \sigma_z \approx 10 \sigma_{r\phi}$)
 $= \frac{\sigma_{r\phi}}{\theta_{\text{stereo}}}$

ADVANTAGES : $\sigma_z \approx 1 \text{ mm}$
 WITHOUT Q MEASUREMENT
 WITHOUT FAST TIMING

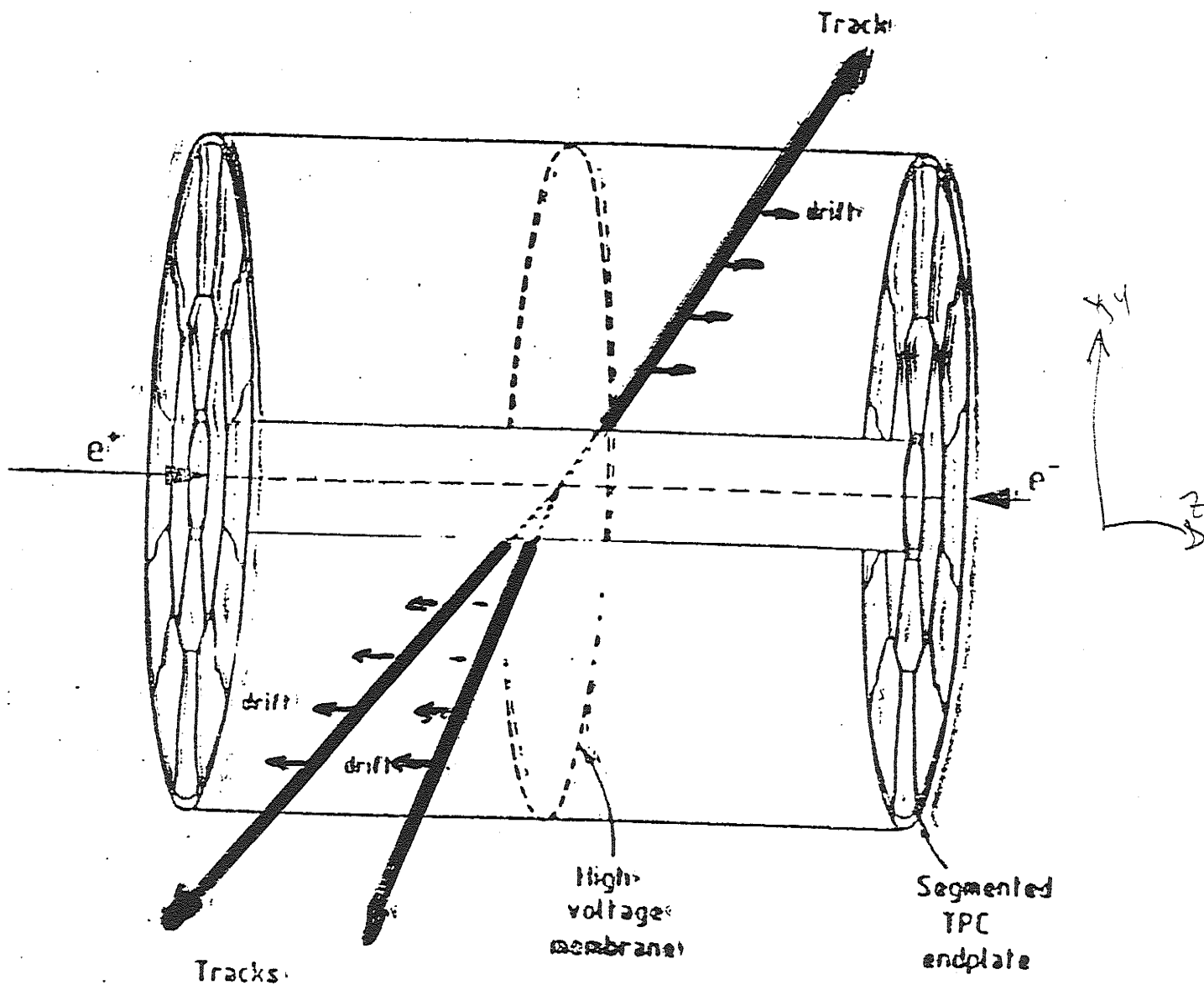
DISADVANTAGES : INFORMATION ONLY AVAILABLE WHEN
 TRACK FOUND IN AXIAL WIRES.

PATTERN RECOGNITION COMPLICATED
 \Rightarrow TIME CONSUMING \Rightarrow NOT AVAILABLE
 ONLINE.

$\theta_{\text{SCT}} = 40\text{mrad} \quad \sigma_z = 25 \quad \sigma_{r\phi} = 1.2\text{mm}$

TIME PROJECTION CHAMBER (ALEPH, DELPHI)

ILD



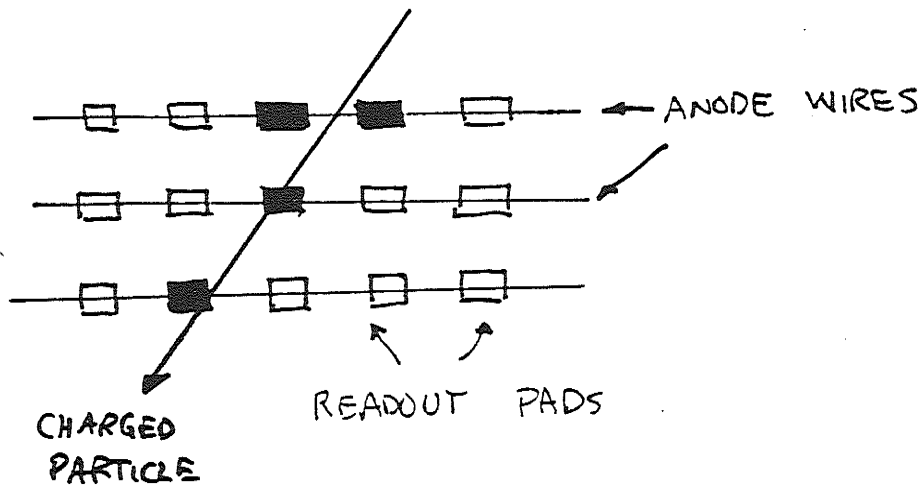
- MEASURE z, θ FROM DRIFT TIME
- MEASURE r, ϕ FROM PADS & WIRES READOUT ON END PLATES

EFFECTIVELY DIVIDE SPACE INTO 3D PIXELS

⇒ GOOD FOR PATTERN RECOGNITION IN
MEDIUM MULTIPLICITY ENVIRONMENTS.

7)

PAD/WIRE READOUT ON ENDPLATES



- WELL ADAPTED TO COMPLEX TOPOLOGIES
- BASE PATTERN RECOGNITION ON PADS.
- WIRES NECESSARY FOR SIGNAL AMPLIFICATION / AVALANCHE BUT CAN SUFFER MULTI-HITS \Rightarrow PATTERN RECOGNITION CONFUSED

OFTEN ADD "EXTRA WIRES" \Rightarrow MANY SAMPLES OF LANDAU DISTRIBUTION FOR ISOLATED TRACKS (SEE PARTICLE ID LATER)



ENORMOUS NUMBER OF CHANNELS FOR PADS (COMPARED TO $2N$ FOR CROSS-WIRES)

BUT GIVES 3D INFO SO PERHAPS NOT SO WASTEFUL.

N^2
↓

USE C.C.D.s TO BUFFER INFO.

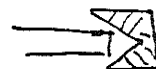
DRIFT TIME CALIBRATION

TPCs PROVIDE MOST STRINGENT REQUIREMENT ON DRIFT DISTANCE VS. TIME RELATIONSHIP.

I.P.

1) USE UV LASERS (e.g. NITROGEN
 $\lambda = 330 \text{ nm}$
 $E = 3 \text{ eV}$)

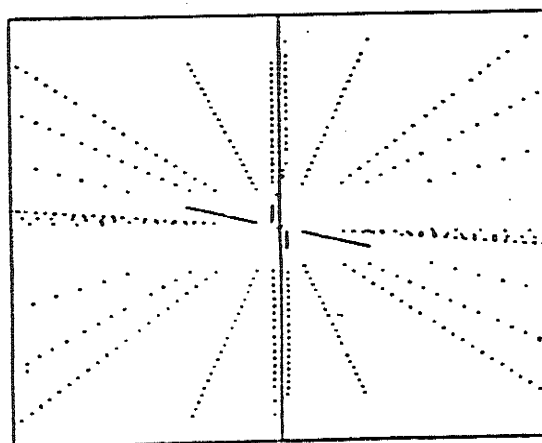
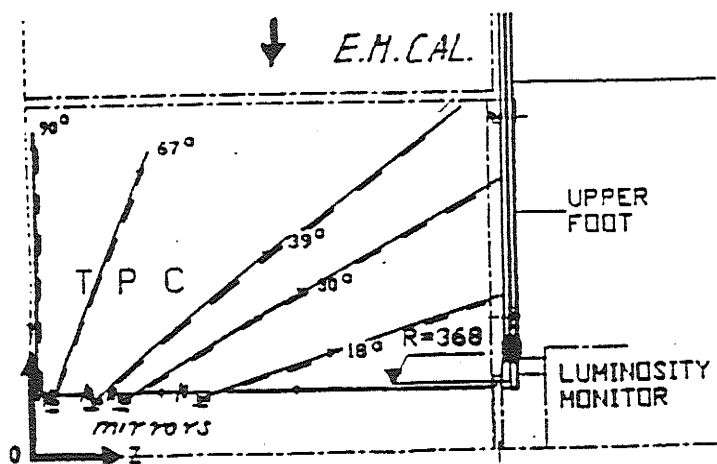
- ADVANTAGES:
- INSENSITIVE TO $|\vec{B}|$
 - " MULTIPLE SCATTERING
 - NO LANDAU FLUCTUATIONS
 - PULSE HEIGHT ADJUSTABLE
 - TWO TRACK RESOLUTION



PROBLEM: $E_{\text{LOW}} > E_Y$

\Rightarrow 2 γ PROCESSES OR IONIZING UN-INTENTIONAL IMPURITIES.

ALEPH

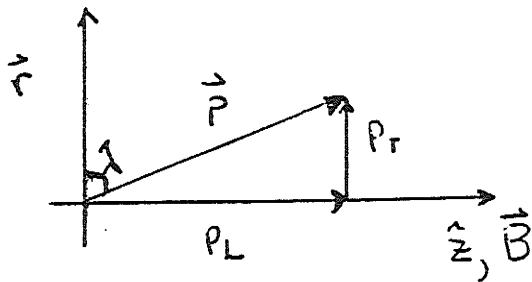


3)

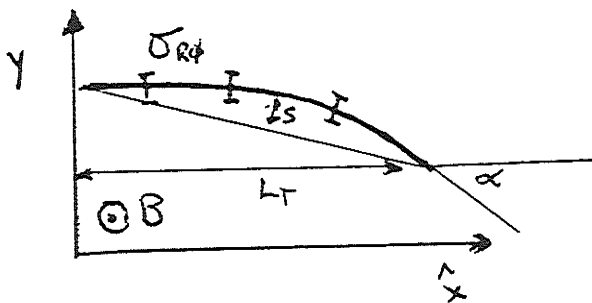
Include in 2024

MOMENTUM MEASUREMENT

CHARGED PARTICLE FOLLOWS HELICAL TRAJECTORY IN MAGNETIC FIELD (TAKE EXAMPLE OF SOLENOIDAL MAGNETIC FIELD)



$$p_T = p \cos \lambda$$



$$p_T = 0.3 B \cdot R_T$$

[GeV/c] [T] [m]

$$Q=1$$

Can approximate:

$$S \approx \frac{L_T^2}{8R_T}$$

$$\alpha \approx \frac{L_T}{R_T}$$

(GLUCKSTERN NIM24 (1963) 381)

MOMENTUM RESOLUTION

$$\begin{aligned}
 \left(\frac{dp}{p}\right)^2 &= \left(\frac{\sigma_{R\phi} a_n}{L_T^2 0.3B}\right)^2 P_T^2 && \text{From } \sigma_{R\phi} \text{ on } S \\
 &+ \left(\frac{\sigma_z f_n \sin\lambda \cos\lambda}{L_T}\right)^2 && \text{From } \sigma_z \text{ on } \lambda \\
 &+ \left(\frac{0.053}{B \beta \cos\lambda \sqrt{L_T X_0}}\right)^2 && \text{From MULTIPLE SCATTERING}
 \end{aligned}$$

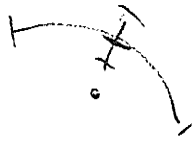
→ FOR EVENLY SPACED MEASUREMENTS (BEST FOR MULTIPLE SCATTERING)

n	3	12	100	n	n > 10
a _n	9.8	6.6	2.6	$\sqrt{\frac{720(n-1)^3}{(n-2)n(n+1)(n+2)}}$	$\sqrt{\frac{720}{(n+4)}}$

→ FOR n/2 MEASUREMENTS IN "MIDDLE"
 n/4 MEASUREMENTS AT ± L_T/2

$$a_n' \approx \sqrt{\frac{256}{n}} \Rightarrow 40\% \text{ TO BE GAINED IF MULT. SCATT NOT A PROBLEM}$$

EXAMPLES



$$\frac{dP_T}{P_T} = \frac{\sigma_{R\phi}}{S}$$

FOR 3 POINTS

$$\frac{dP_T}{P_T} = \frac{P_T}{0.3B} \frac{\sigma_{R\phi} a_n}{L_T^2} \approx 1\% P_T$$

$L_T = 1m$
 $B = 1T$
 $n = 3$
 $\sigma_{R\phi} = 300\mu m$

$$\frac{dP_T}{P_T} = 0.1\% P_T \quad \text{CDF}$$

$1 - 100 GeV$

$L_T = 1.35m$
 $B = 1.4T$
 $n = 100$
 $\sigma_{R\phi} = 300\mu m$

$$\frac{dP_T}{P_T} = 0.1\% P_T \quad \text{DELPHI}$$

$1 - 20 GeV$

$L_T = 1.5m$
 $B = 1.2T$
 $n = 20$
 $\Rightarrow \sigma_{R\phi} = 150\mu m$

$$\frac{dP_T}{P_T} = 0.01\% P_T \quad \text{ATLAS}$$

↑ OPTIMISTIC

$a_{10}' = 5.0$

$10 - 1000 GeV$

$L_T = 1.1m$
 $B = 2T$
 $n = 10$

$\Rightarrow \sigma_{R\phi} = 19\mu m$

OTHER TERMS ?

(2)

$$f_n = \sqrt{\frac{12(n-1)}{n(n+1)}}$$

$$n=10 \Rightarrow f_n \approx 1$$

$$n=100 \quad \approx 0.3$$

$$\sin \lambda \cos \lambda \leq 1/2$$

$$\sigma_z \lesssim \text{mm}$$

\Rightarrow SECOND TERM
 $\lesssim 10^{-3}$ INDEPENDENT OF p

(3)

$$\left(\frac{dp}{p}\right)_{\text{m.sc.}} = \frac{0.053}{B\beta \cos \lambda \sqrt{L \cdot \chi_0}}$$

$$\beta = v/c$$

$$B=1\text{T}$$

$$L=1\text{m}$$

$$\chi_0(\text{Ar}) = 14.0\text{cm}$$

$$(\text{Air}) = 36\text{cm}$$

$$(\text{CO}_2) = 28\text{cm}$$

$$(\text{He}) = 7.6\text{m}$$

$$\left(\frac{dp}{p}\right) = 0.5\%$$

$$\left(\frac{dp}{p}\right) = 0.1\%$$

IF YOU ARE WORRIED ABOUT TRACKS THIS WILL DOMINATE 0.1 — 1.0 GeV/c

CHOOSE He (CLEO III, BABAR, ...)

(14)

ELECTRON DRIFT IN ($\vec{E} \times \vec{B}$)

FOR (\vec{E}) CONSTANT IN GASES

EQUATE ACCELERATION

$$\frac{\vec{v}_D}{\tau} + \frac{e}{m_e} (\vec{B} \times \vec{v}_D) = \frac{e\vec{E}}{m_e}$$

τ = MEAN TIME BETWEEN COLLISIONS

$$\Rightarrow \vec{v}_D = \frac{\mu(E)}{1 + \omega^2 \tau^2} \left(\vec{E} + \frac{\vec{E} \times \vec{B}}{|\vec{B}|} \omega \tau + \frac{(\vec{E} \cdot \vec{B}) \vec{B}}{|\vec{B}|^2} \omega^2 \tau^2 \right)$$

$$\omega = \frac{e|\vec{B}|}{m_e} \quad (\text{cyclotron Frequency})$$

FOR: $\omega \tau \ll 1$

ELECTRONS FOLLOW (\vec{E}) CO_2

$\omega \tau \gg 1$

ELECTRONS FOLLOW (\vec{B}) Ar/CH_4

TYPICALLY A MIXTURE!

LORENTZ ANGLE

$$V_x = \mu E_x \frac{1}{(1 + \omega^2 \tau^2)}$$

$$\vec{E} = (E_x, 0, 0)$$

$$\vec{B} = (0, 0, B_z)$$

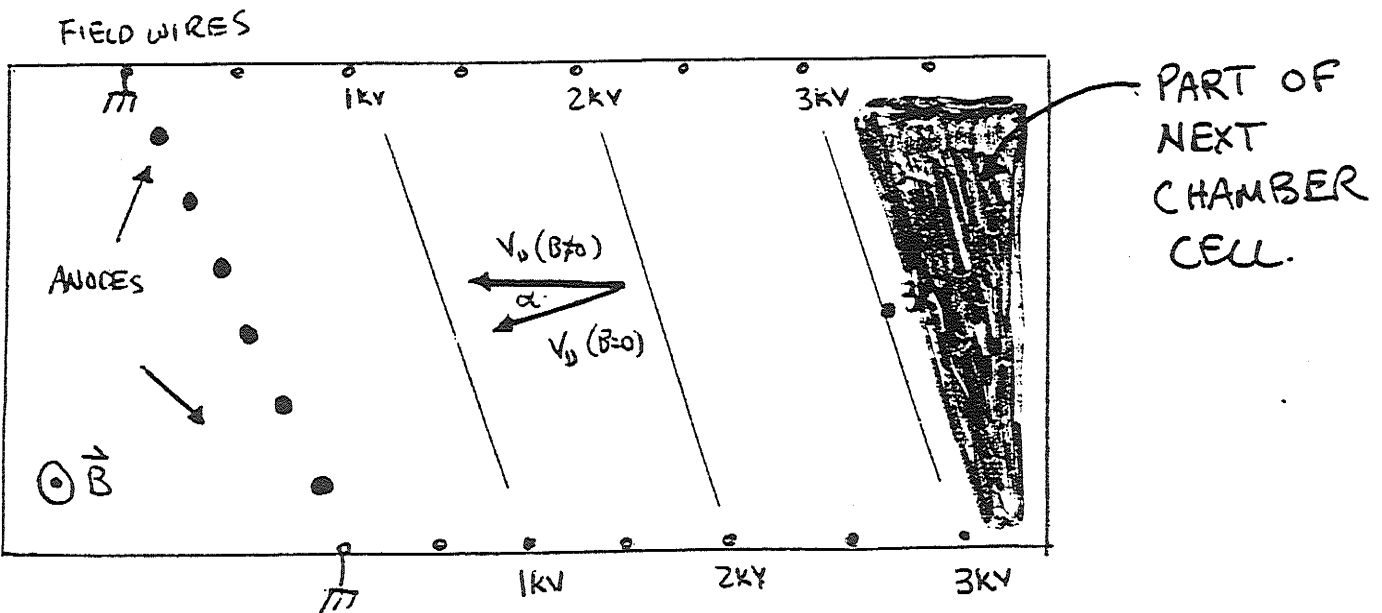
$$V_y = -\mu E_x \frac{\omega \tau}{(1 + \omega^2 \tau^2)}$$

$$\begin{aligned} \Rightarrow V_D &= \sqrt{V_x^2 + V_y^2} = \mu E_x \frac{1}{\sqrt{1 + \omega^2 \tau^2}} \\ &= \mu E_x (\cos \alpha_L) \end{aligned}$$

$$\tan(\alpha_L) = \omega \tau \quad (\text{LORENTZ ANGLE})$$

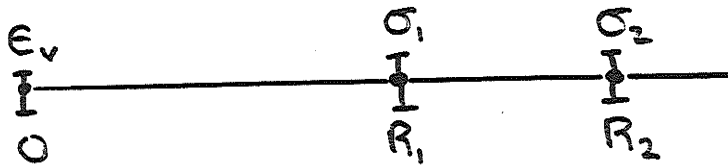
USEFUL 1ST APPROXIMATION

COMPENSATE WITH SKEWED ELECTRIC FIELD



Impact Parameter Resolution

Can be derived from simple extrapolation of a line/propagation of uncertainties:



$$E_v = \sqrt{\left(\frac{R_1 \sigma_2}{(R_2 - R_1)}\right)^2 + \left(\frac{R_2 \sigma_1}{(R_2 - R_1)}\right)^2} = \sqrt{R_1^2 + R_2^2} \frac{\sigma}{\Delta R}$$

Lessons:

- i) Make R_1 as small as possible.
- ii) Make σ as small as possible.
- iii) Make R_2 as large as possible.

When particle crosses material it scatters adding additional error in estimating the impact parameter.

$$\Theta_{\text{SCATTER}} \approx \frac{14}{P(\text{GeV})} \sqrt{\frac{F}{X_0}} \quad (\text{mrad})$$

$$E_v^{\text{SCATTER}} \approx \frac{1 \text{ mrad}}{P} \cdot R_1$$

FOR TYPICAL
BEAMPIPE +
FIRST SILICON
LAYER @
1% X_0

SPECIFIC EXAMPLES

THE DELPHI TRACKER (ACTUAL PERFORMANCE)

1) 3 LAYERS SILICON MICROSTRIPS ($r = 6 - 11 \text{ cm}$)

$$\sigma_{r\phi} \approx 8 \mu\text{m} \quad \text{per point}$$

$$\sigma_{rz} \approx 13 - 25 \mu\text{m} \quad (\text{FUNCTION OF } \theta)$$

2) 24 WIRE JET CHAMBER ($r = 12 - 23 \text{ cm}$)

$$\sigma_{r\phi} = 40 \mu\text{m} \quad (\Sigma' 24 \text{ points})$$

3) 5 LAYERS OF STRAW TUBES ($r = 24 - 28 \text{ cm}$)

DESIGNED AS A TRIGGER

4) TPC WITH 16 PAD ROWS ($r = 40 - 110 \text{ cm}$)

$$\sigma_{r\phi} = 250 \mu\text{m}$$

$$\sigma_{rz} = 880 \mu\text{m} \quad (\text{over } \approx 1.34 \text{ m drift drift})$$

5) 5 LAYERS OF PROPORTIONAL TUBES

CROSS-CHECK OF TRACK OUTSIDE R.I.C.H.

RESULTS (DELPHI TRACKER)

① IMPACT PARAMETER RESOLUTION:

- DOMINATED BY SILICON

$$\sigma_{r\phi}^{\text{track}} = 20 \mu\text{m}$$

$$P_T \approx 5 \text{ GeV}/c$$

$$\sigma_z^{\text{track}} = 60 \mu\text{m} \quad (\text{at } 90^\circ)$$

(OTHER DETECTORS CONTRIBUTE < 10% TO I.P. WEIGHT)

② MOMENTUM RESOLUTION

$$\frac{\sigma_p}{p} = (0.6 \times 10^{-3}) p \quad (p \text{ in GeV}/c)$$

NB: TPC ALONE $\Rightarrow 7 \times 10^{-3}$

SILICON + OUTER TUBES $\Rightarrow L_{\text{TRACK}} \quad 0.7\text{m} \rightarrow 1.9\text{m}$

$$\Rightarrow \left(\frac{\sigma_p}{p^2} \right)_{\text{TOTAL}} \rightarrow \left(\frac{0.7}{1.9} \right)^2 \left(\frac{\sigma_p}{p^2} \right)_{\text{TPC}}$$

$$\leq 1 \times 10^{-3}$$

$$\Rightarrow \text{SILICON (1 TUBES)} \quad \sigma_{r\phi} < 250 \mu\text{m}.$$

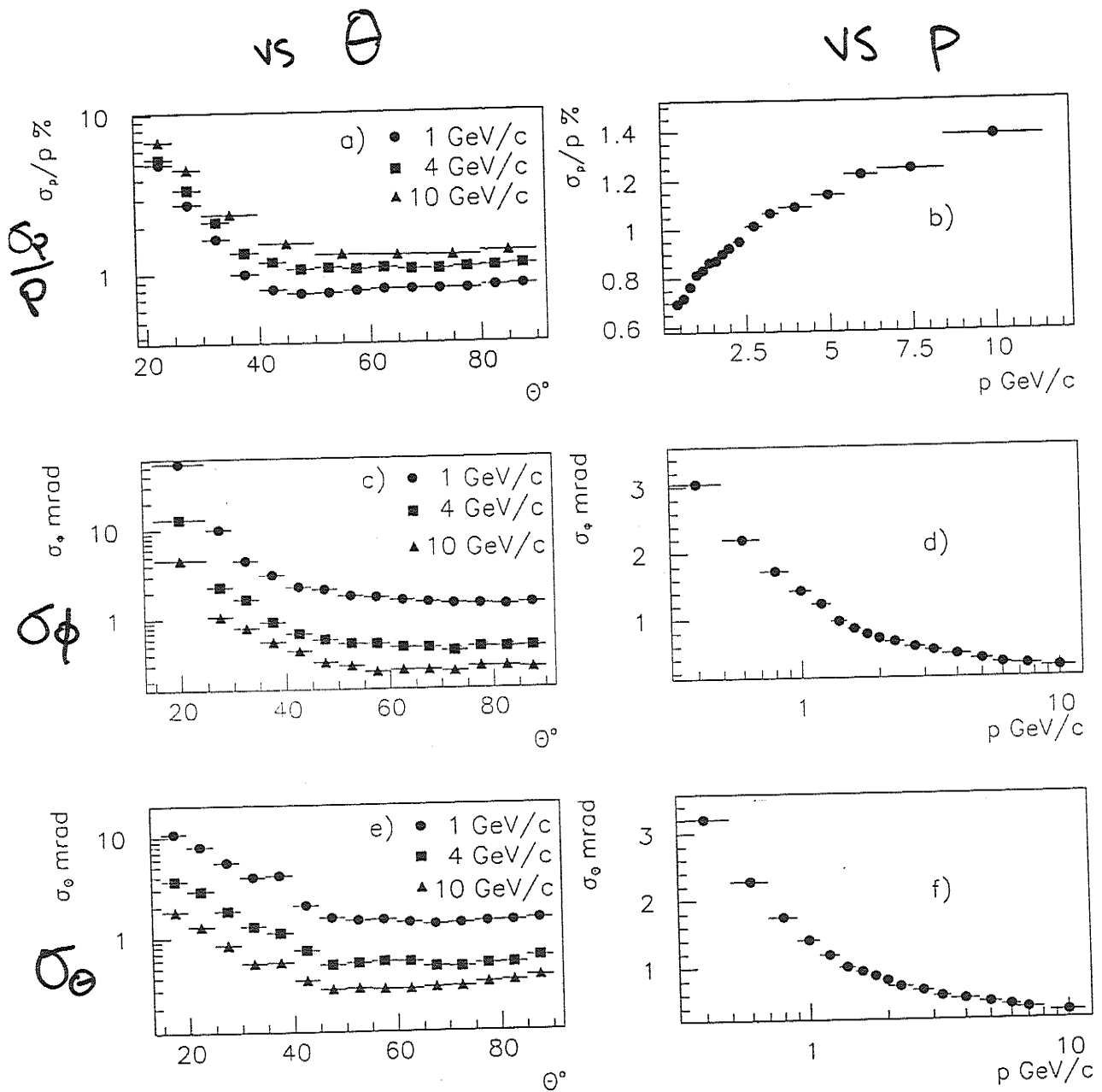
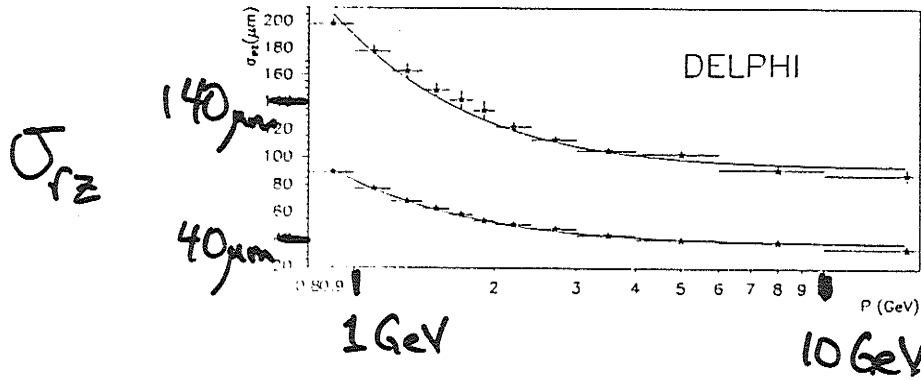
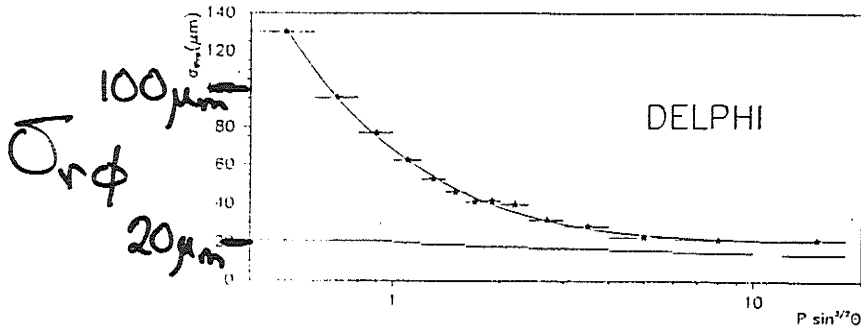


Figure 9: Track parameter precisions estimated by comparing simulated and reconstructed parameters: (a) momentum precision as a function of the polar angle θ , (b) momentum precision as a function of the momentum for barrel tracks, (c) azimuthal angle precision as a function of θ , (d) azimuthal angle precision as a function of the momentum for barrel tracks, (e) polar angle precision as a function of θ , (f) polar angle precision as a function of the momentum for barrel tracks.

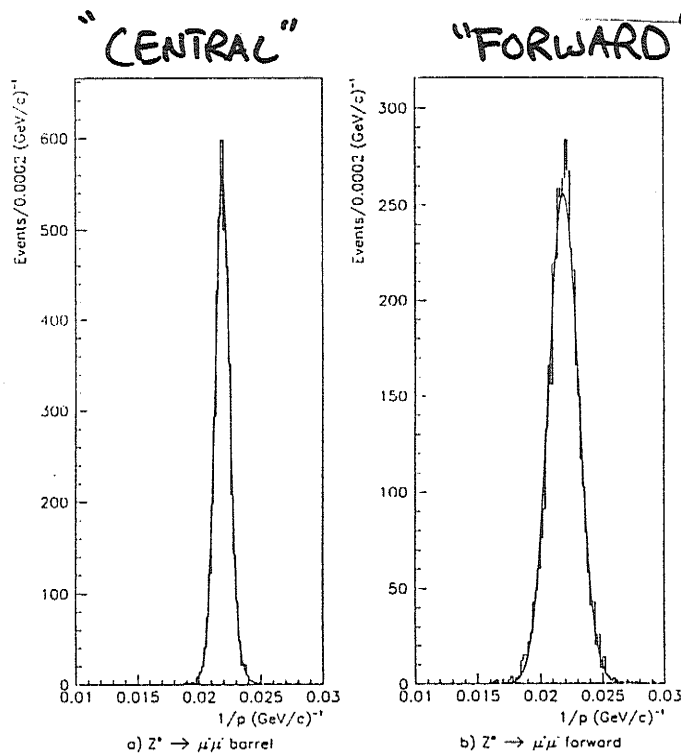
IMPACT PARAMETER RESOLUTION



MOMENTUM RESOLUTION

$\theta(^{\circ})$	Detectors	$\sigma(1/p)(\text{GeV}/c)^{-1}$
≥ 42	VD+ID+TPC+OD	0.6×10^{-3}
≥ 42	ID+TPC+OD	1.1×10^{-3}
≥ 42	VD+ID+TPC	1.7×10^{-3}
≥ 36	VD + FCB included	1.3×10^{-3}
25-30	FCB included	1.5×10^{-3}
< 25	FCB included	2.7×10^{-3}

Table 4: Momentum measurement precision for 45.6 GeV/c muons.



THE ATLAS TRACKER (PROJECTED PERFORMANCE)

1) 2 LAYERS SILICON PIXELS ($r = 11.5 - 17.5 \text{ cm}$)

→ MOSTLY FOR PATTERN RECOGNITION $\frac{1}{3}$ RAD.
HARDNESS

→ $\sigma_{r\phi} \approx 15 \mu\text{m}$ (PITCH = $50 \mu\text{m}$)

2) 4 LAYERS SILICON STRIPS ($r = 30 - 60 \text{ cm}$)

$\sigma_{r\phi} \approx 25 \mu\text{m}$

(PITCH = $85 \mu\text{m}$)

$\sigma_{rz} \approx 800 \mu\text{m}$

($\theta_{\text{STEREO}} = 2.3^\circ$)

3) 35 LAYERS OF STRAWS ($r = 63 - 107 \text{ cm}$)

INTER STRAW REGION FILLED WITH TRANSITION
RADIATOR (ELECTRON IDENTIFICATION)

$\sigma_{r\phi} = 150 \mu\text{m} / \text{STRAW}$ (7 mm DIAMETER STRAWS)

ALSO GIVES MANY LAYERS OF \approx CONTINUOUS
TRACKING HITS \Rightarrow "IMPROVED" PATTERN
RECOGNITION.

Modified tracker layout

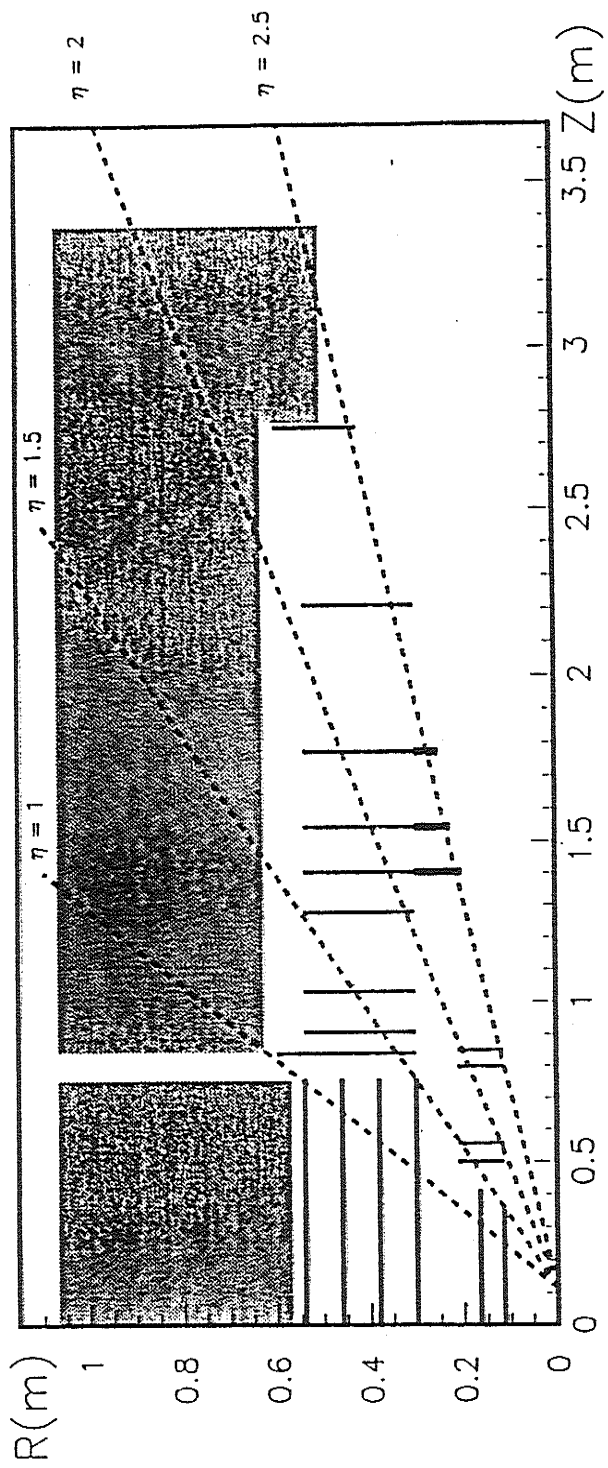
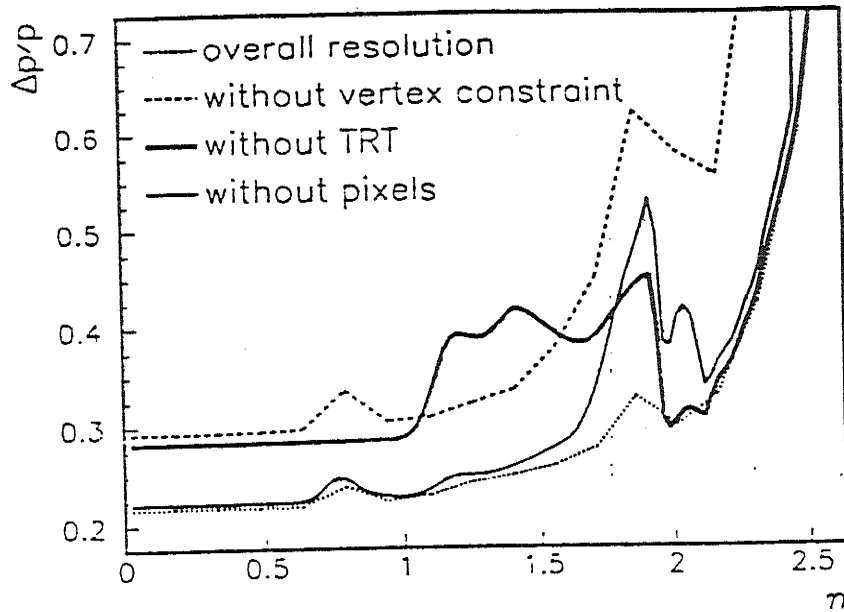


Figure 3.23: Conceptual layout of the silicon option for the forward precision tracking. Thin lines represent silicon detectors, while thicker lines represent GaAs detectors.

RESULTS (FROM SIMULATIONS)



$\sigma_{p_T} = 0.04\% p_T$
 \uparrow
 $\geq 3\times$ BETTER THAN CDF

Figure 3.35: Robustness of the momentum resolution versus η for muons of $p_T = 500$ GeV

Table 3.14: Parametrized impact-parameter resolution of the ATLAS inner detector for the barrel part of the various vertexing layouts described in the text. The resolutions are given as functions of p_T in GeV and of the polar angle, θ .

Vertex detector	σ_{ip} (μm)	σ_z (μm)
High luminosity	$27 \oplus \frac{220}{p_T \sqrt{\sin \theta}}$	$130 \oplus \frac{240}{p_T \sqrt{\sin \theta}}$
Binary pixels	$18 \oplus \frac{61}{p_T \sqrt{\sin \theta}}$	$84 \oplus \frac{130}{p_T \sqrt{\sin \theta}^3}$
Analog pixels	$12 \oplus \frac{52}{p_T \sqrt{\sin \theta}}$	$52 \oplus \frac{79}{p_T \sqrt{\sin \theta}^3}$
Micro-strips	$13 \oplus \frac{62}{p_T \sqrt{\sin \theta}}$	$39 \oplus \frac{90}{p_T \sqrt{\sin \theta}^3}$